

Technical Report # 5-32279
Contract Number NAS8-36955
Delivery Order No. 51

**COMPLEX BURN REGION
MODULE (BRM) UPDATE
(5-32279)**

Final Technical Report for the Period
November 01, 1989 through September 30, 1990

(February 1991)

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(NASA-CR-184296) COMPLEX BURN REGION MODULE
(CBRM) UPDATE Final Technical Report, 1 Nov.
1989 - 30 Sep. 1990 (Alabama Univ.) 68 p

CSCL 211

N92-20681

Unclass
0078065

G3/28

NASA

National Aeronautical and
Space Agency

Report Document Page

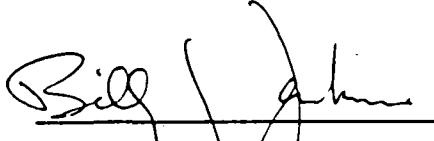
1. Report No. 5-32279	2. Government Accession No.	3. Recipient's Catalog No.
4. Title and Subtitle Complex Burn Region (CBRM) Update for the Solid Rocket Internal Ballistics Module (SRIBM) Program for the ASRM Design Performance Assessments		5. Report Due 30 September 1990
7. Author(s) Mr. Carl Adams, Dr. Billy Jenkins		6. Performing Organization Code Research Institute, UAH
9. Performing Organization Name and Address UAH Research Institute RI E-47 Huntsville, AL 35899		8. Performing Organization Report No.
12. Sponsoring Agency Name and Address National Aeronautics and Space Administration Washington, D.C. 20546-001 Marshall Space Flight Center, AL 35812		10. Work Unit No. D.O. 51
		11. Contract or Grant No. NAS8-36955
		13. Type of report and Period covered Final Technical Report February 1991
		14. Sponsoring Agency Code
15. Supplementary Notes		
16. Abstract Complex Burn Region Module (CBRM) Update for the Solid Rocket Internal Ballistics Module (SRIBM) Program for the ASRM Design/Performance Assessments. Develop an improved version of the solid rocket internal ballistics module program that contains a diversified complex region model for motor grain design, performance prediction, and evaluation.		
17. Key Words (Suggested by Author(s)) Solid Propellant, Burn Module, ASRM		18. Distribution Statement
19. Security Class. (of this report) Unclassified	20. Security Class. (of this page) Unclassified	21. No. of pages 19 + Appendices
22. Price		

PREFACE

This technical report was prepared by the staff of the Research Institute, The University of Alabama in Huntsville. It documents the research performed under contract NAS8-36955, Delivery Order 51. Mr. Carl Adams and Dr. Billy Jenkins were Principal Investigators. Technical work was accomplished by Billy Jenkins, Mr. Mark Bowden, and Dr. Larry Dunbar. Mr. Douglas Blackwell, Propulsion Laboratory, provided technical coordination.

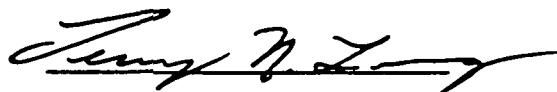
The views, opinions, and/or findings contained in this report are those of the author(s) and should not be construed as an official National Aeronautics and Space Administration, Marshall Space Flight Center position, policy, or decision unless so designated by other official documentation.

I have reviewed this report, dated Feb. 1981 and the report contains no classified information.



Principal Investigator

Approval:



Research Institute

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1. Nature of the Task

The design of solid rocket motors requires the prediction of the burning surface area and the port volume in the motor as a function of burn time. Alternatively, if the grain regression rate is specified, the burnback distance as a function of time can be found and the burning area and port volume calculated in terms of burnback distance, reducing the problem to one of solid analytical geometry.

MSFC has been using the Complex Burning Region Model (CBRM) and the computer code based upon this model since the early 1970s when it was developed for them by Northrop Services specifically to aid in the design of the Revised Solid Rocket Motor (RSRM) referred to today as the SRM. At the present time, a replacement for the RSRM is being designed, the Advanced Solid Rocket Motor (ASRM). The ASRM differs in grain design from the SRM to the extent that the CBRM is no longer adequate to predict its performance. Both the ASRM and the SRM use grain designs wherein, aft of the head dome, a star pattern section is followed by a cylindrically perforated (CP) section with an intermediate transition zone. As presently envisioned, the CP section of the ASRM is not qualitatively different from that of the SRM; it is the star and transition regions which have changed. Figures 1 and 2 contrast the differences between the two motors. Instead of a simple star, as seen in the SRM, the ASRM introduces a compound star wall consisting of three surfaces instead of one (Fig. 1). The transition region, instead of a simple "climb out" from the star valley, widens as it progresses towards the CP region introducing new surfaces (Fig. 2). (Numerical dimensions for nominal cases are given in the appendix.)

This report describes the effort, performed under contract to MSFC, which modifies the CBRM to be applicable to the ASRM and the results achieved. The code produced will be referred to as CBRM-A.

2. Approach

The exact dimensional configuration of the ASRM is subject to change. Consequently, care was taken to insure that the modified CBRM code has the flexibility to correctly calculate burning area and port volume for variations on the ASRM design first provided to UAH in May 1990. This flexibility, and the increase in the number of surfaces, constitute the principal analytical complication introduced by the new grain pattern. Familiarity with the original CBRM documentation (Refs. 1 and 2), terminology, and code will be assumed in this report. CBRM-A was coded to provide for the minimum change in input, output, and program flow from that of CBRM.

a. Extent of the flexibility in CBRM-A.

Figure 3 shows the convention used in referring to the star and transition surfaces in the ASRM. Note that as regression proceeds, the concave intersection where S2 and S3 meet will develop into a cylinder. This cylinder will be called CY1. In fact, for coding purposes each of the surfaces has an alternate designation. The section on coding gives the

FIGURE 1
COMPARISON OF RSRM AND ASRM STAR SECTION GRAIN PATTERN

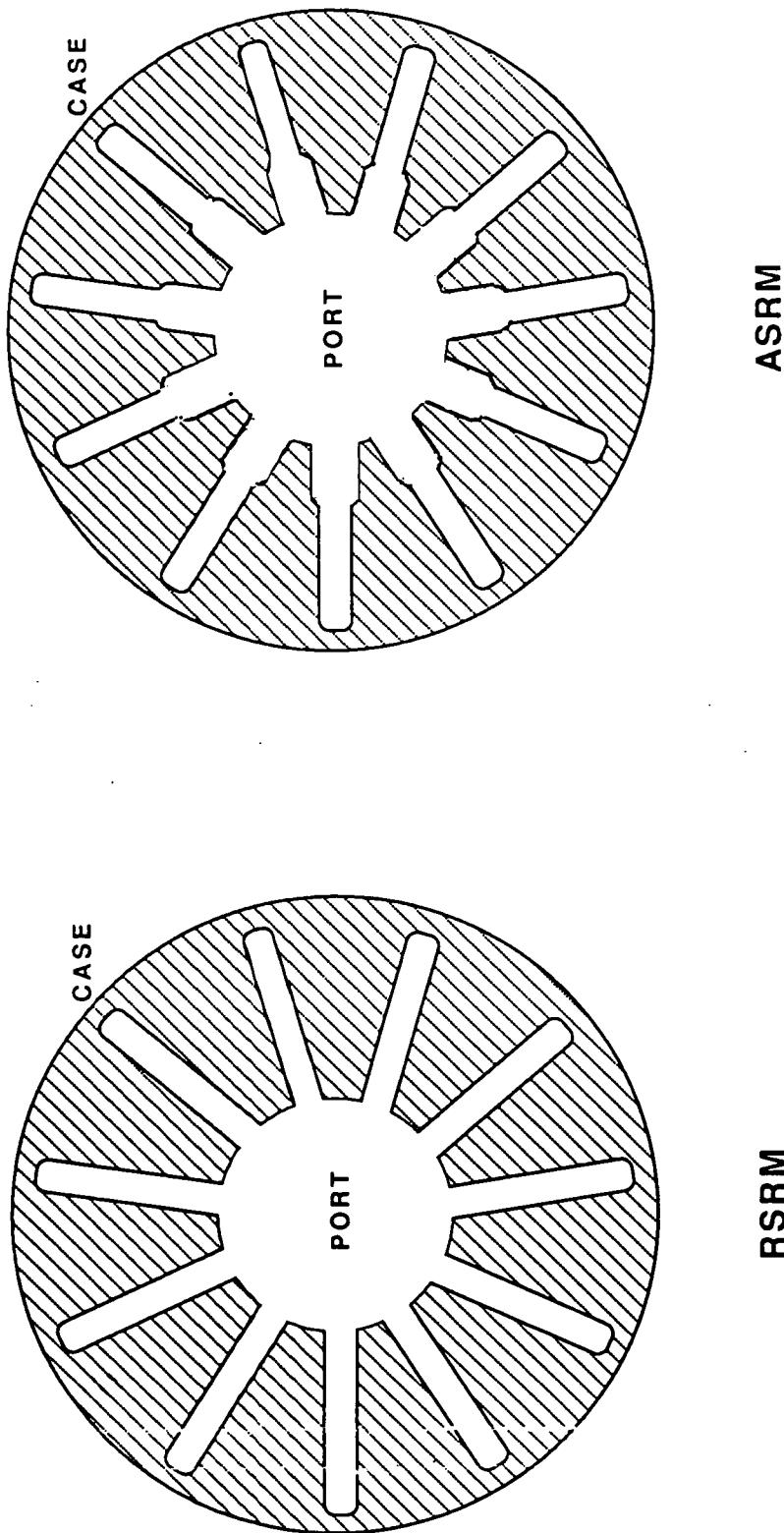


FIGURE 2

COMPARISON OF RSRM AND ASRM TRANSITION REGION CONFIGURATION

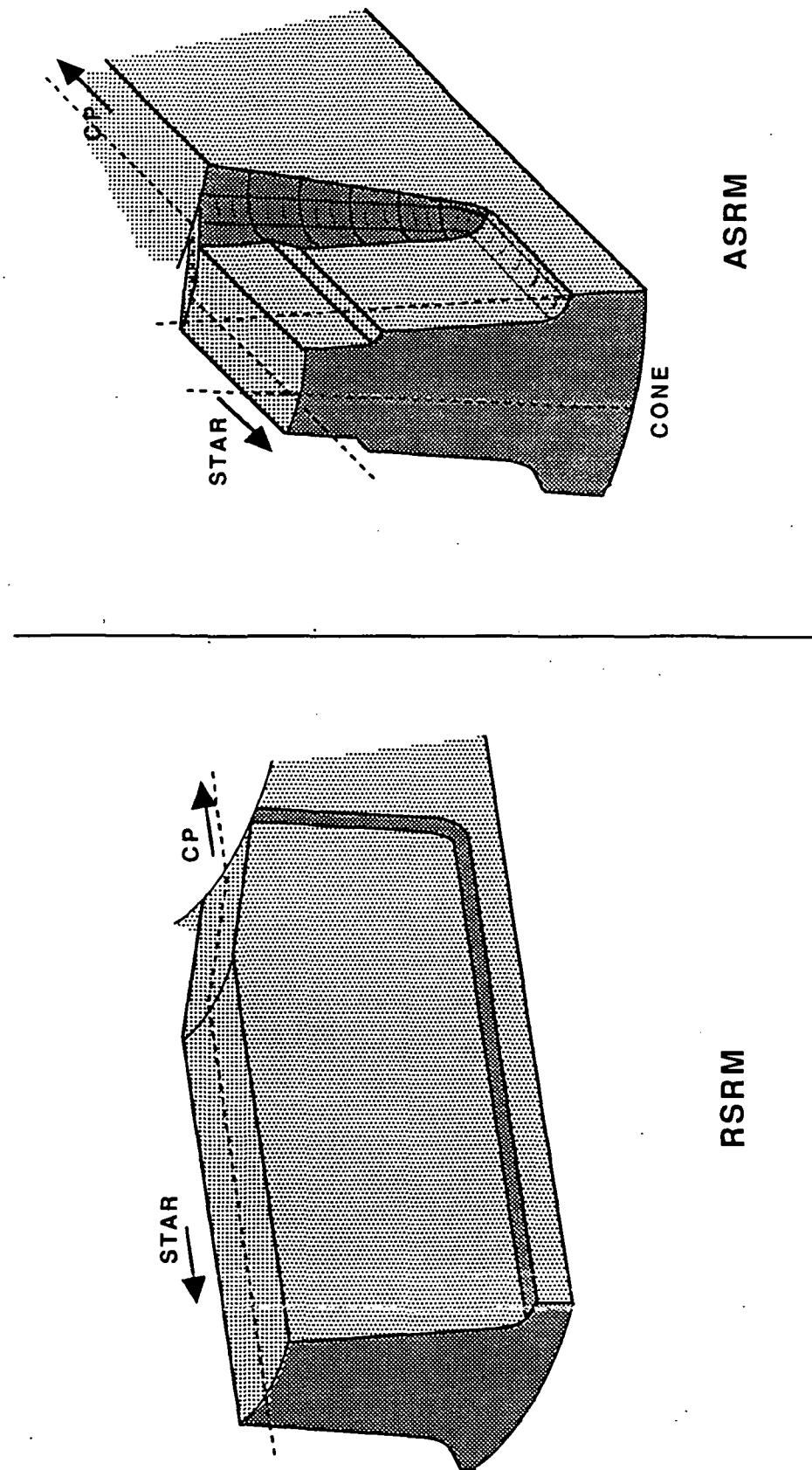
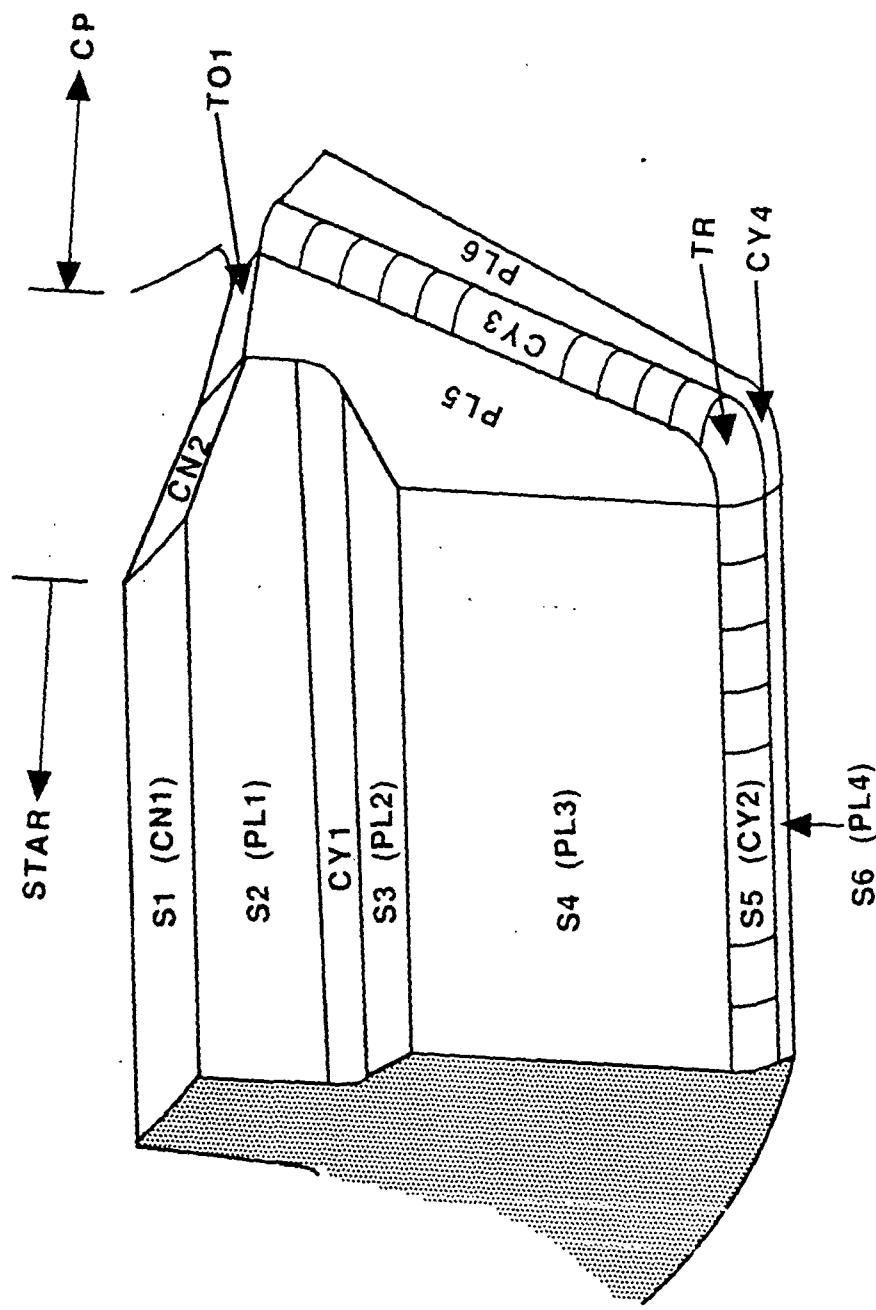


FIGURE 3
DESIGNATION OF SURFACES IN THE STAR AND TRANSITION REGIONS



correspondence between the S-designation and the more descriptive one used in the code. Although the grain configuration shown in the ASRM drawing has the surfaces S2 and S4 parallel to the valley centerline in cross section, it is not necessary for this to be true for CBRM-A. The only constraint is that, before ignition, S2, S3, and S4 be continuous planes throughout the star region. The valley floor, comprised of S5 and S6, need not be (and in the ASRM is not) continuous in this region. If a simple star geometry is desired, the surfaces S2 and S3 can be made null by the proper input. The transition region, on the other hand, must consist of the surfaces as shown in the ASRM drawing, but all angles and dimensions may vary from those shown. In order to benchmark the CBRM-A against the CBRM, it would be necessary to insert code to avoid zero denominators in the computation of the intersection of the star wall surfaces with transition surface S7.

While CBRM appeared to account for burnback rates which were a function of axial station, z , the code did not actually incorporate this. CBRM-A has implemented this feature in the star region.

b. Introduction of new surfaces

The number of possible ways in which surfaces may intersect increases as the factorial of the number of surfaces. The actual computation of the lines of intersection is simple, but the logic to determine the sequence of events during regression becomes quite complicated, particularly if the flexibility mentioned above is to be maintained. The following section, Coding, goes into more detail on this.

c. Surface representation

To facilitate the representation of surfaces, both initially and during the course of burn, standard representations for each class of surface were used which differ somewhat from Ref. 1. In each case, the surface is described by a number of constants, one of which need only have the cumulative burnback distance added to it to account for regression. The same coordinate system is used as in CBRM. The cumulative burnback distance is S_b . The standard representations are as follows:

- Plane (S2, S3, S4, S6, S7, S9)

$\bar{r} \cdot \hat{n} = R_p + S_b$ where $\bar{r} = (x, y, z)$ and \hat{n} is a unit vector normal to the plane in the direction of regression. This becomes $\alpha x + \beta y + \gamma z = R_p + S_b$ where α , β , and γ are the direction cosines of the unit normal, $\alpha^2 + \beta^2 + \gamma^2 = 1$. R_p is the perpendicular distance from the origin to the plane before ignition.

- Cone centered on z-axis (S1, S8)

$x^2 + y^2 = \left(z \tan \alpha_c + \frac{R_c + S_b}{\cos \alpha_c} \right)^2$ where α_c is the cone semivertex angle and R_c is the perpendicular distance from the origin to cone surface before ignition. If α_c should be zero, a cylinder results.

- Cylinder (CY1, S5, S11)

$$\frac{[Ax + Cy - (A^2 + C^2)z + (AB + CD)]^2}{A^2 + C^2 + 1} + [Cx - Ay + (AD - BC)]^2 = (A^2 + C^2)(R_{cy} + S_b)^2$$

where the axis of the cylinder is defined by the equations: $x = Az + B$, $y = Cz + D$, and the initial radius of the cylinder is R_{cy} . This equation is not valid if the cylinder axis is perpendicular to the z-axis, as is the case with S10. Axis flexibility is not required of S10 and its equation can be written knowing only its initial radius and its center x and y values. It is worth noting that the equation for the cylinder as given in Ref. 1 is incorrect.

- Torus ringing the z-axis (S12)

$$(\sqrt{x^2 + y^2} - R_{maj})^2 + (z - ZTO)^2 = (R_{min} + S_b)^2 \text{ where } R_{maj} \text{ is the large radius of the torus, } R_{min} \text{ is the minor radius of the torus, and } ZTO \text{ is the z-station of the torus (input).}$$

S13 is a sector of an oblate skewed toroid which is better handled without attempting to represent it by an equation.

The user is not expected to supply the constants used to represent the various surfaces. The required input is, for the most part, in terms of quantities given on the ASRM drawings and is cast into the proper form by the code.

3. Coding

a. General comments

The program flow of CBRM-A has not changed qualitatively from that of CBRM. In brief, MAIN (PROGRAM CBRM-A) has been changed to accept the new input (see Appendix A) and the references to incremental dividing planes (IDPs) have been changed to correspond to the new division of the transitional region. Whereas the CBRM called subroutine PLNSET to initialize the grain configuration tables and place the IDPs, an additional subroutine, TRNSET, is called to initialize the transition region. MAIN contains the major loop which increments time and prints the variables of interest as time progresses. The computation of the incremental burning areas and port volumes between IDPs is governed by subroutine BNCTRL. BNCTRL sets the burnback rate (a constant was used in CBRM) for the time increment and calls the appropriate subroutine (STRBRN, TRNBRN, SLTBRN, or CPBURN) to calculate the new cross section at the IDP after regression over the time increment and return the incremental burning areas and port volumes which, through labelled COMMON are passed to MAIN. BNCTRL has only been changed to reflect the changed IDP placement in the transition region. The changes to CBRM-A do not affect any of the burnback routines except STRBRN, TRNBRN and their attendant subordinate routines. These routines will be described later.

Although the CBRM was purported to accept a burnback rate varying with z, the coding to properly treat the resulting uneven regression at each IDP was absent. This has been added to CBRM-A for the star region, although it is inhibited in the compiled version. In MAIN a constant, IBRNCON, is set to zero, causing the program to skip the recomputation

of the surfaces. If IBRNCN is non-zero, this recomputation is carried out, requiring considerably more computation time. No functional form for the dependence of burning rate with z is provided for. When this option is required it will only be necessary to recompile with IBRNCN not equal to zero, specify the dependence of burning rate with z , modify the COMMON block BRNCN to convey this to BNCTRL, and enter the functional form (or table) at the indicated point in BNCTRL.

Supplement 1 to this report is a listing of the CBRM-A including numerous comments to guide the user through the modifications to the code. Those parts of the code dealing with the aft, slot, and CP sections have not been changed. The following list indicates the subroutines eliminated by the modifications, all of which dealt with the CBRM star and transition regions.

SAREA2

FILLET

PSTN1

PSTN2

TRBRN2

SETIDP

The changes to MAIN and BNCTRL have been outlined above. The next list covers the other changed routines, the new routines subordinate to these and a qualitative description of the changes. The comments in the listing in Appendix A will indicate to the reader where these changes occur in the code.

- PLNSET Up to the point where the setting of IDPs in the CP region and at the slots in the CP region begins, this subroutine has been changed completely. The constants for the generalized equation for each of the surfaces in the star region before motor ignition are calculated and set into arrays. In the CBRM, all the variables necessary to describe the star section at each IDP were entered into array CALCON. A new array, STRNU, is used to store the additional parameters necessary to describe the altered star region. For coding purposes, the surface nomenclature used in Figure 3 is changed in the arrays to reflect the type of surface. The correspondence is as follows. The first time a particular type of surface appears (cone, cylinder, or plane), the order of storage of the constants in the arrays is given.

S1 CN1(IDP, K) , K=1 for α_c , K=2 for R_0

CY1(K), K=1 to 4 for A,B,C, and D; K=5 for R_{cy}

S2 PL1(IDP, K), K=1,2,3 for alpha, beta, and gamma, K=4 for R_p

S3 PL2(IDP, K)

S4 PL3(IDP, K)

S5 CY2(RFPL, K)

S6 PL4(IDP, K)

The above list indicates the subscripts of the arrays. The cones and the planes must be allowed to change for each IDP in case the burnback rate is not constant. Cylinders, on the other hand, do not experience a change in axis or initial radius due to non-constant burning rates. Consequently, CY1 remains constant throughout the star region by the assumption of continuity of surfaces S2 and S3 throughout the star region. CY2, however, may change at intermediate reference planes (RFPL). New subroutines written to support PLNSET include STPTST (to be described later), PLANE and SOLVE which use three given points on the plane surfaces to derive the constants for the PL_ arrays, and KISS and PT20 to solve for the point where a line going through a given point is tangent to a given circle.

- TRNSET This is an entirely new subroutine. PLNSET still sets all the initial IDPs, but TRNSET sets up the constants defining the initial surfaces in the transition region. Some iteration is called for since the information given in the drawing does not allow one to determine the axis of S11 in closed form. Instead, the width of the aft end of the transition is given (WIDCO in the input) along with the z-position of the end of transition and enough information to determine the equation of S9. This, and the cross section at the end of the star section is enough to define S11 in standard form. The other surfaces, save unlucky S13, can then be defined in a straightforward manner. The correspondence between the surfaces as discussed in this report and the arrays containing the standard constants for the surface are as follows:

S7 PL5

S8 CN2

S9 PL6

S11 CY3

S12 TO1(K) K=1 for ZTO, K=2 for R_{maj}, and K=3 for R_{min}

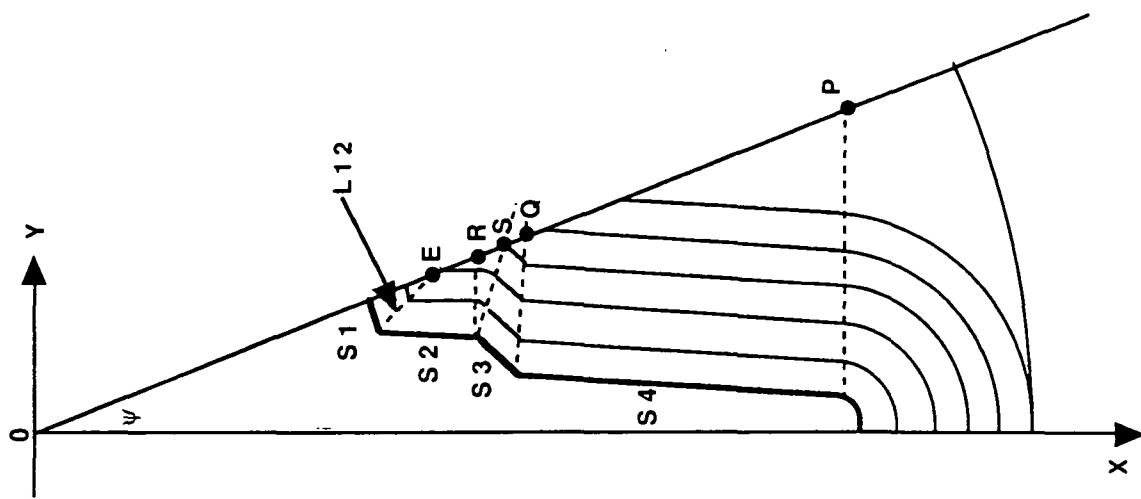
b. Treatment of star region

The star region is treated in much the same manner as it was in CBRM, i.e., subroutine STRBRN calls STRGEO which returns the burning perimeter and port cross-sectional area for the IDP which are then used by STRBRN to find the incremental burning area and port volume between this and the preceding IDP. STRBRN required little change. If IBRNCON is not equal to zero, subroutine SRESET is called to account for the change in the surface equation constants due to non-constant burning.

STRGEO, however, has been entirely changed. In CBRM-A, as regression proceeds, the order of disappearance of surfaces at each IDP is not a priori known. This can be calculated, and is left to the code. Figure 4 shows certain significant points in the course of regression. Point E marks the disappearance of S1, point R the disappearance of S2, point S the disappearance of CY1, point Q the disappearance of S3, and point P the disappearance of

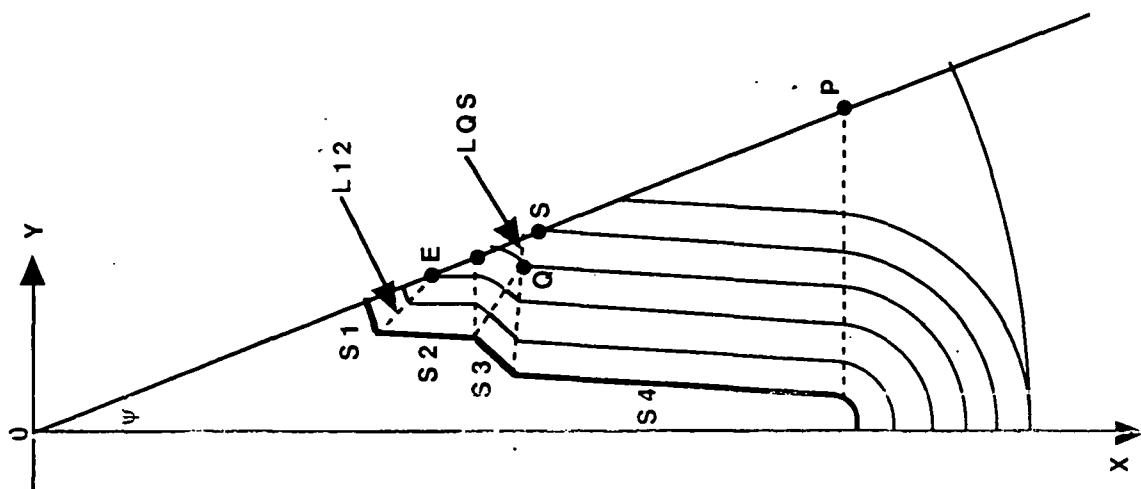
FIGURE 4

SIGNIFICANT REGRESSION POINTS IN A STAR SECTION IDP



4 a

pt E -S1 disappears
 R -S2 "
 S -CYI
 Q -S3 "
 P -S4 "



4 b

S4. The significant points are determined by eliminating the parameter S_b between the equations of each successive pair of surfaces to determine the equation of the burnback line or conic demarcating these surfaces. For example, S1 and S2 can be solved by elimination of S_b , at the z-value for the IDP, to find the burnback parabola L12 (Figure 4). The centerline of the star peak is defined by the line $y=xtan\psi$. If burnback loci intersect this line of symmetry before intersecting each other, the associated point is located at this intersection (Fig. 4a). But if burnback lines intersect (and hence a surface disappears) before reaching the centerline (examine point Q in figure 4b) then a new burnback line is found for the surviving surfaces surrounding the one which disappeared (the burnback ellipse LQS in figure 4b is an example). A subroutine, STPTST, calculates the position of the points E, R, S, Q, and P as well as the value of S_b corresponding to this point for each IDP. If the burnback rate is constant, STPTST is called only once and this is done from PLNSET. If the burning rate is a function of z, STPTST is also called from STRBRN before calling STRGEO. The data relative to each point is stored in arrays PTE, PTR, etc. These arrays are doubly dimensioned, the first being the IDP and the second 1,2 or 3 corresponding to the x,y, and S_b associated with the point. STRGEO can determine the order and time of disappearance of the surfaces by the values of S_b found in these arrays.

As with CBRM, the z location of the end of the star region changes as burning progresses. The number of the last IDP in the star section is designated MIDPL.

c. Treatment of the transition region

In the CBRM, the transition region was divided by six IDPs into seven different regions, not all of which existed at the same time. These were movable IDPs which tracked such locations as the beginning of the CP region or the most forward point of burnthrough to the case. In recoding for CBRM-A, this proved to be impractical due to the complexity of the geometry. The number of possible configurations which the transition region may take for various orientations of the transition and star surfaces is astronomical if flexibility is to be maintained. Figure 5 shows some of the forms assumed by the transition region as it regresses. Consequently, a less elegant, but equally accurate, method was used. In CBRM, in order to calculate the port volume and burning area in the segment delimited by the torus corresponding to S12 (which was bounded by movable IDPs), a numerical integration was used rather than the general prismatic formula. In CBRM-A, a similar approach is used throughout the transition region. The IDP corresponding to the beginning of the CP region is MIDPL+1, so that the entire transition region is contained between the two movable IDPs, MIDPL and MIDPL+1. This region is sliced into parallel layers spaced 0.1 inches with the number of layers determined by the locations of the bounding IDPs. The outline of the remaining exposed propellant grain and outer case in each layer is calculated.

Subroutine TRNSET was called to initialize the planes and bounding IDPs in the transition region. BNCTRL calls TRNBRN, providing it with the accumulated burnback for the transition region. It returns port volume, burn area, and exposed outer case area for the entire transition region.

TRNBRN determines a set of nine key geometric points by calling subroutines P1 through P9. These key points denote intersections of surfaces that compose the transition region. This set is a function of the accumulated burn back and all key points, except P7, are determined by analytically solving three determining surface equations simultaneously. P7,

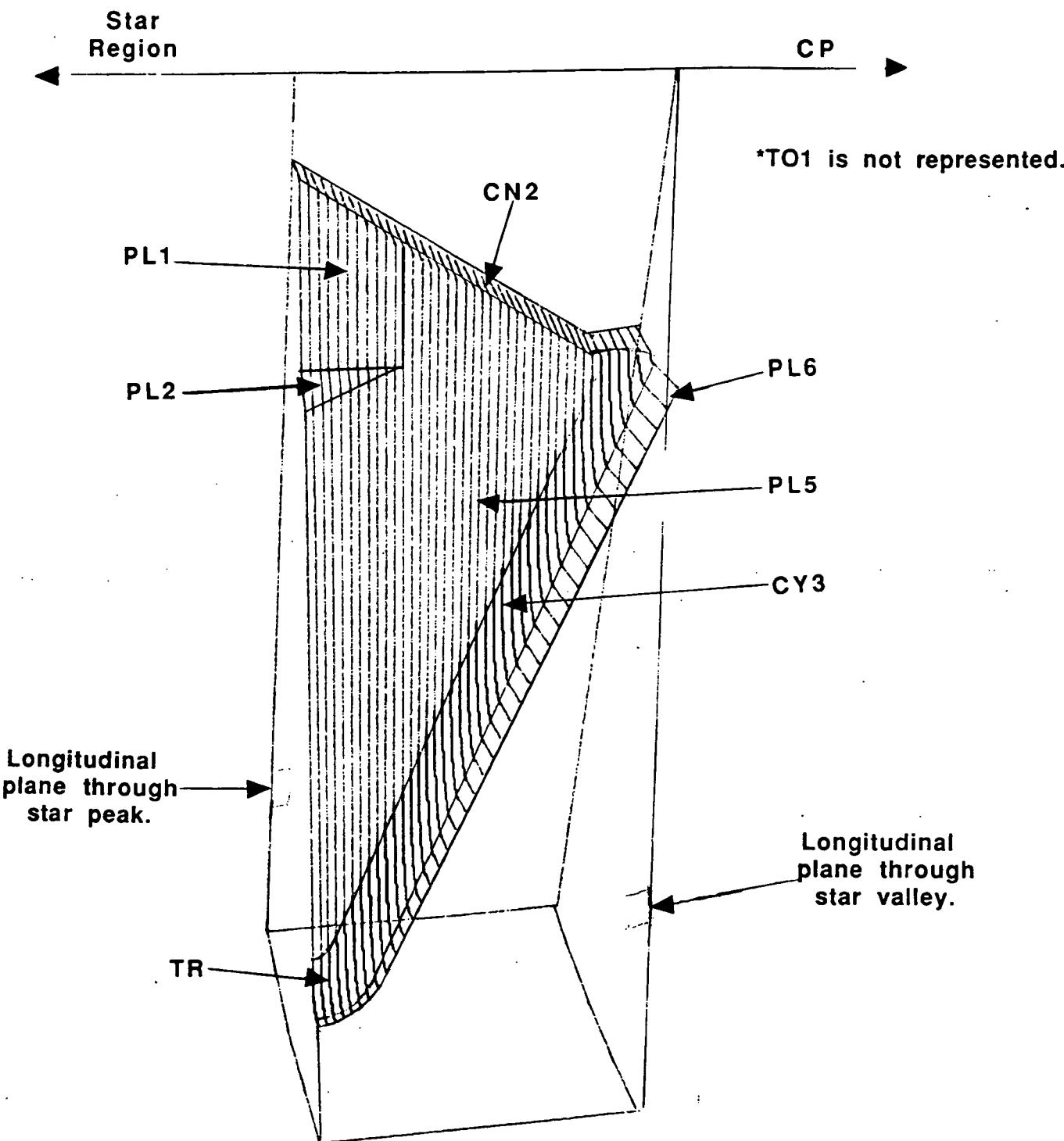


FIGURE 5-a
Transition Region Before Regression

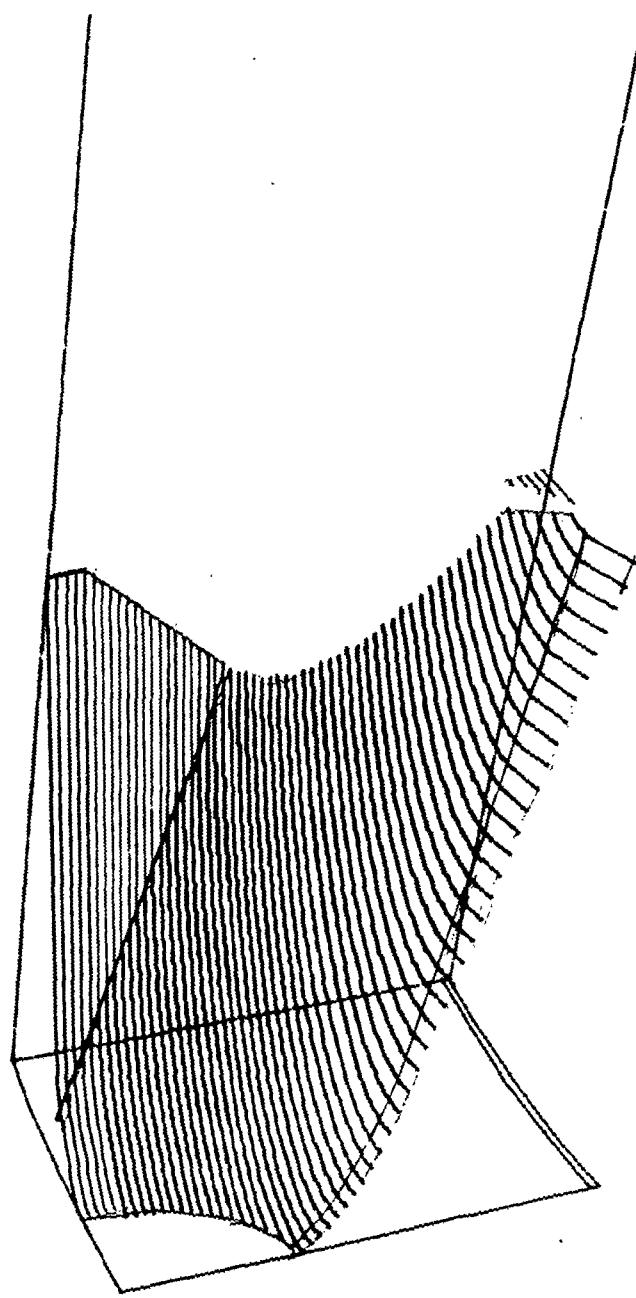


FIGURE 5-b
Transition Region at an Intermediate Stage of
Regression

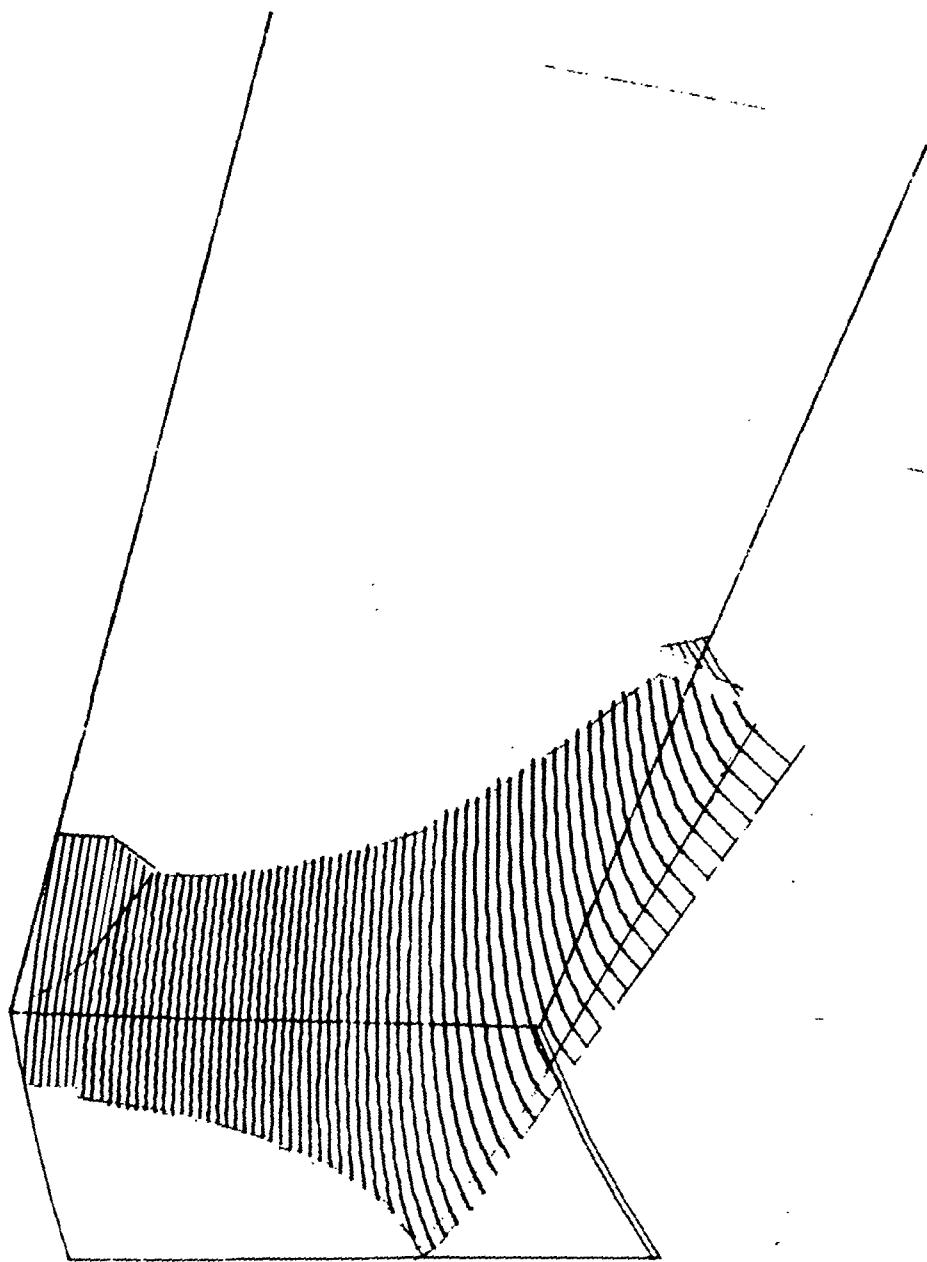


FIGURE 5-c
Transition Region at an Intermediate Stage of
Regression

which is specified in part by a toroidal surface, is determined numerically by sequential testing the axial coordinate at small steps of 0.1 inches. The two off-axial coordinates are determined by analytically solving the determining surface equations.

For each layer, subroutines TS1 through TS13, one for each surface, determine two limits by geometrically correct interpolation algorithms based on the key point set, geometric limits of the outer case and the line of symmetry of the star peak [$y=x \cdot \tan(\psi)$]. The distance between these paired limits specifies the contribution to the outline of the grain. This value is stored in array TS(_). An additional limit point is determined that specifies the surface boundary with the exposed case. The distance between this point to the star valley centerline is the outline of a layer at the outer case. This value is stored in array TC(_). The burnback area and outer case area are determined by numerical integration of the outline of the grain and outer case for each layer across the transition region. Port volume, in turn, after the initial volume is determined by numerical integration in subroutine PORTV, is determined sequentially by numerical integration of burn area for repeated calls of TRNBRN.

TRNBRN also provides the z-values of MIDPL and MIDPL+1, separating the transition from star region and the transition from the CP region, respectively.

In the current implementation of the program, the torus S12 is not represented but the cone CN2 and the CP port are assumed to join without a fairing transition (see figure 5). Moreover, an approximate relation is used to represent the surface S13 in order to facilitate solution of its intersection with other surfaces.

4. Results

CBRM-A has been run using the most recent version of the ASRM geometry and compared with manual calculations of the intial port volume and burning area in the star and transition regions. The appendix describes the input to this sample case. In order to assess the limitations of the code, the parameters defining the geometry were varied within reasonable bounds. The results of these robustness studies are described in supplement 2 to this report.

Figures 6a through 6c show the burning area as regression proceeds for various mass addition regions of the example. After about 38" of regression, the transition surfaces begin to disappear, and the logic for determining the sucession of intersections momentarily fails. This causes the anomalous spike in the burning area curve seen in figure 6b. The magnitude and extent of this spike is not large.

5. Further remarks

By using some of the new subroutines, the computation of the slot burning and aft region burning could be streamlined. In addition, none of the mass addition regions, save the star region, account for non constant burn rate. This can be added in a rather straightforward way.

Figure 6a
Fuel surface area, star region

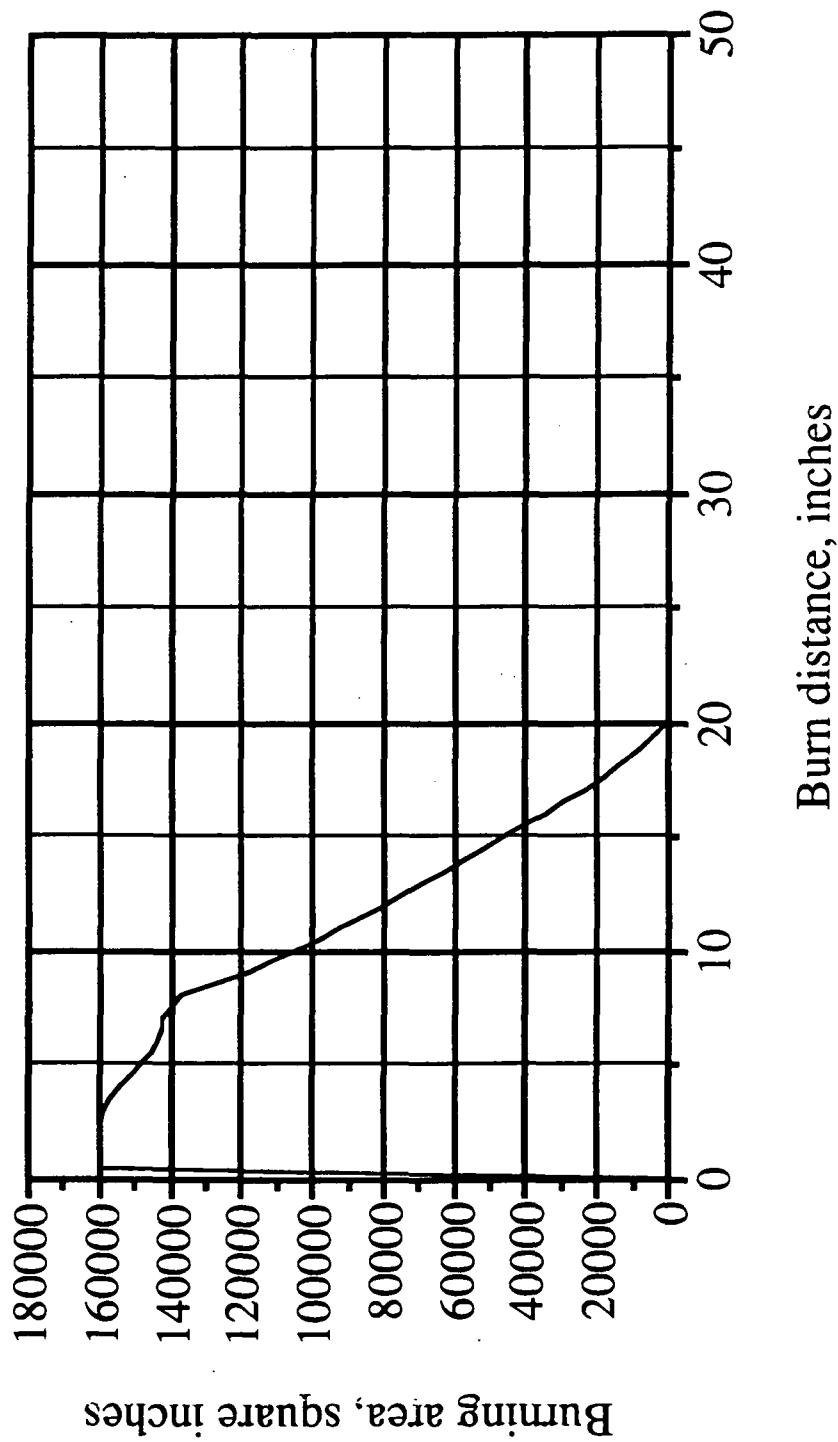


Figure 6b
Fuel surface area, transition region

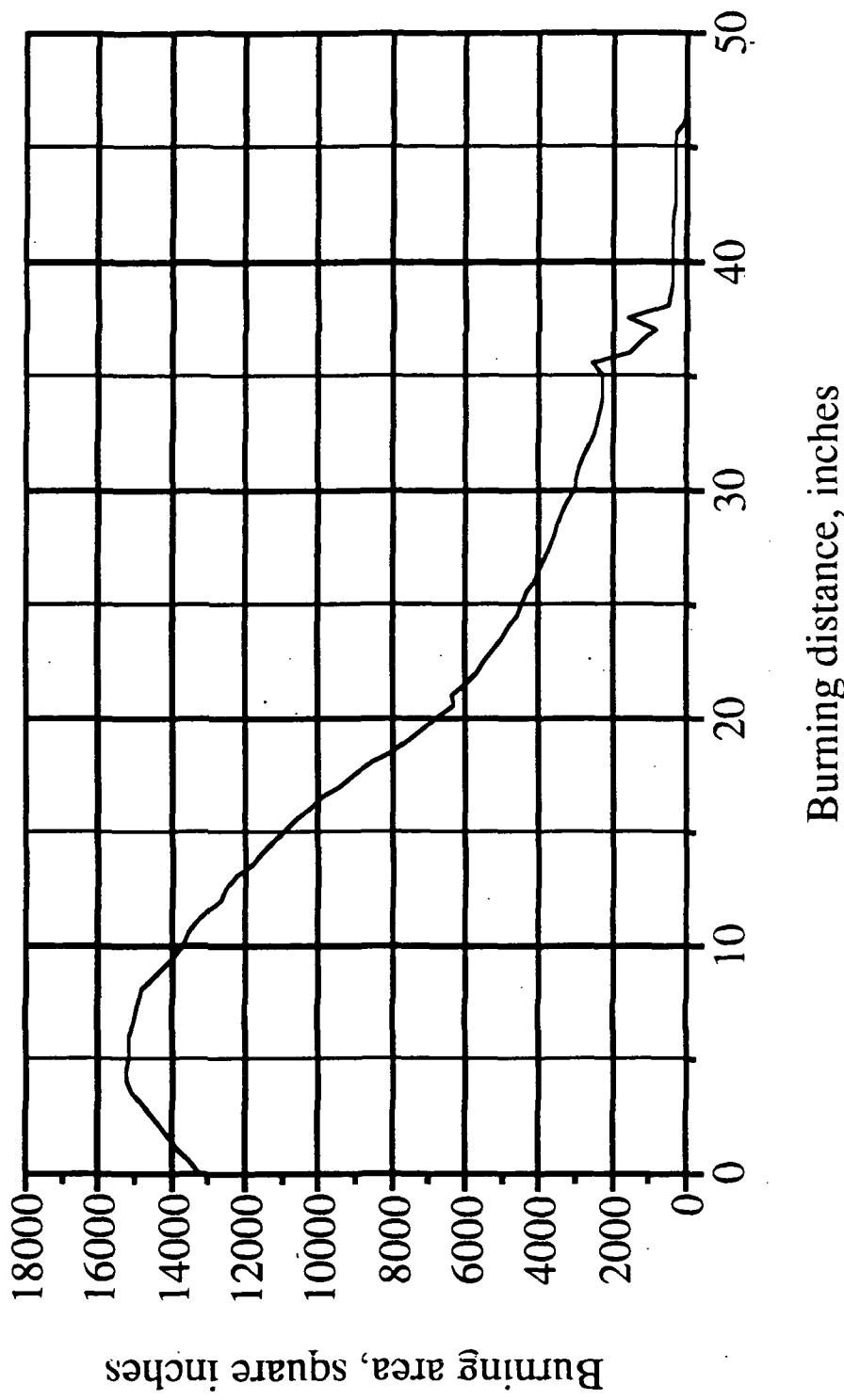
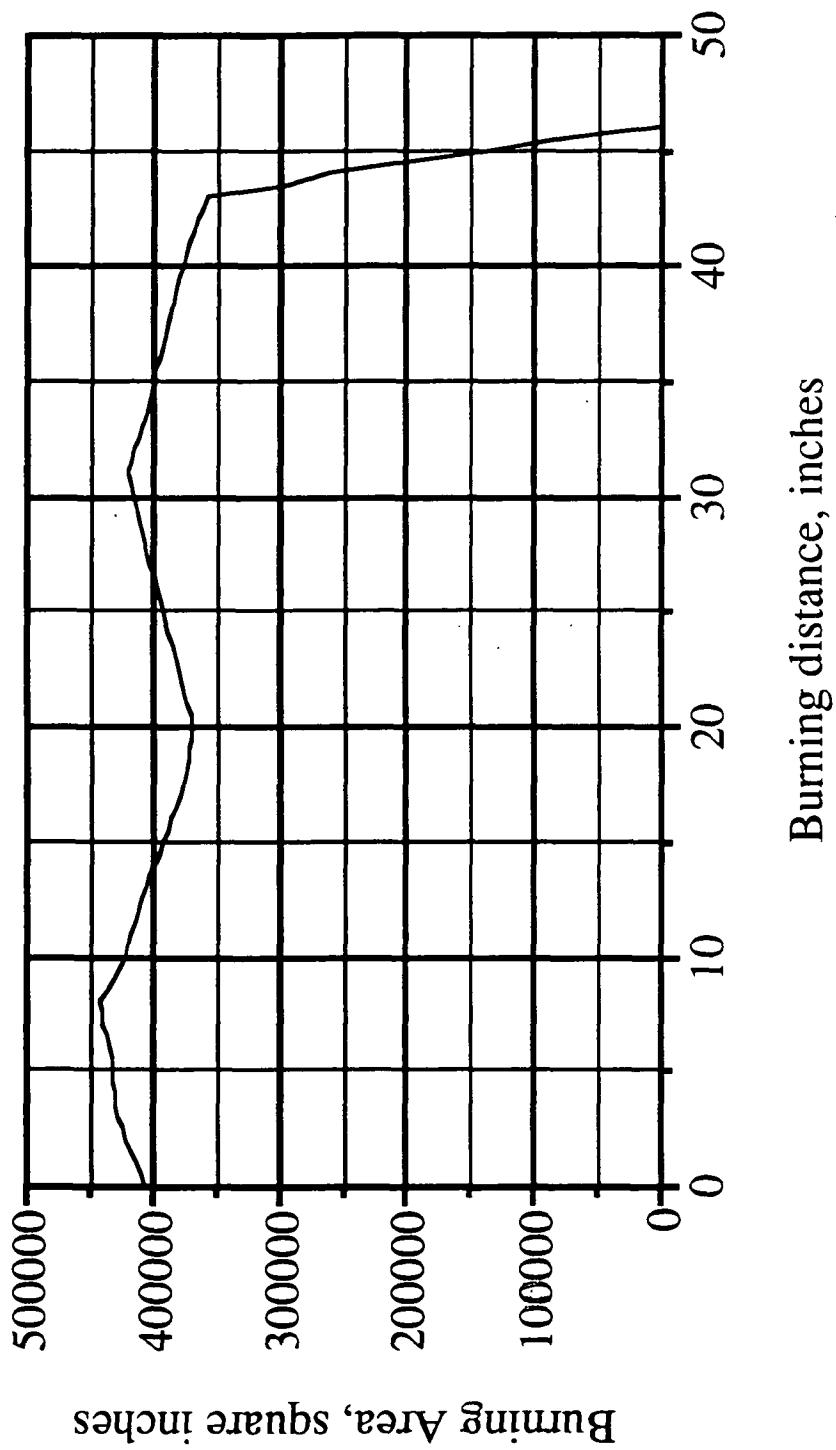


Figure 6c
Fuel surface area between both tangent planes



While a great deal of effort has been devoted to making CBRM-A flexible, it is by no means a general purpose program. It should be able to handle all simple variations on the ASRM propellant grain using the current concept as a baseline. If additional surfaces are incorporated into the design, some recoding will be necessary. Computer Aided Design (CAD) software such as the BRL-CAD provides an alternative way of accomplishing what the CBRM family of programs does by combinatorial geometric means and offers a greater flexibility for readily changing configurations.

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2. Winkler, J. C., and Kingsbury, J. A., "*Users (sic) Manual for the Solid Rocket Booster Internal Ballistics Module (SRIBM2)*", Northrop Services, Inc., Huntsville, Alabama, TR-225-1787, April 77.

APPENDIX A

DESCRIPTION OF INPUT AND AN EXAMPLE WITH OUTPUT LISTING

1. Contents of the Appendix

This appendix begins with a general discussion of the input expected by the CBRM-A code. This is followed by a listing of the input corresponding to the most recent iteration on the configuration for the ASRM as of the publication of this report. This listing annotates the new input and changed input. A partial listing of the output is also included.

2. Input to code

Familiarity with the input to CBRM is assumed. The differences and additions caused by modifying the program to the CBRM-A version are stressed. All input is still achieved with the namelist IB2DAT.

a. Placement of reference planes

Figure A1 represents a longitudinal section of the star and transition sections of a hypothetical grain configuration which can be handled by CBRM-A. Reference planes may be inserted as needed to describe the star region geometry. The NRFth reference plane is set at the end of the star region. The arrays have been dimensioned to accommodate up to 10 reference planes in the star section (NRF<11). The reader is reminded that the initial configuration of the star region is constrained so that planes S2, S3 and S4 must be continuous throughout the star region. The following reference plane, number NRF+1, is placed at the beginning of the CP region - there are no intervening ones. CBRM-A thus does not require as many reference planes in the transition region as did CBRM. The ASRM concept requires only 4 reference planes throughout the star and transition regions; one at the forward tangent plane, one at the discontinuity in the slope of the case, one at the end of the star region, and the fourth plane is the one which introduces the pure CP region.

The quantities which are input through the reference plane array remain the same; its z-coordinate, port radius, radius of valley floor, and case radius.

b. Introduction of new star region variables

Figure A2 depicts cross sections of the star region at its beginning (reference plane 1), and at its end (reference plane NRF). The RSRM star valley was of constant width whereas the ASRM valley may taper with z. Consequently, the CBRM input quantity RTOPTP was replaced with the two quantities RTOPTF and RTOPTA, identified in the drawing. The x-coordinates of the valley wall discontinuities at both the forward and aft ends of the star region are given (XHIF, XLOF, XHIA, XLOA) are given, but the y-coordinates are only given at reference plane NRF. This avoids overspecifying the surfaces by assuring that only three points are given or determined in each of the three planes, S2, S3, and S4 which are assumed to be continuous throughout the star region before burning starts.

c. Introduction of new transition region variables

Figures A1 and A3 illustrate the quantities which must be provided to CBRM-A to define the transition region. In CBRM, the variable α_4 was an input. From drawings of the new geometry it is seen that the value of z at the end of the transition region, reference plane NRF+1, the radius of the climb-out arc, R3, and the reference plane data at NRF are adequate and α_4 is not explicitly input. The fillet radius in the climb-out corners is assumed to be the same as that in the corners of the star valleys (FR). The width of the flare at the aft end of the transition region, WIDCO in figure A3, completes the description of the transition region.

d. Range of geometric parameters yielding credible solutions

To check robustness of the code, the grain regression was modelled and graphically depicted to see if the propellant surface followed a reasonable course during burning while the geometric parameters were varied within reasonable limits. In many cases it was necessary to vary more than one input variable in order to keep the input consistent.

- Star Valley Floor Radius

The star valley floor radius (RVF) was increased by both two, six, and eight inches without difficulty; however, problems were encountered when RVF was decreased by over three inches from the nominal case, because the valley floor got so close to the case that point P (figure 4) was no longer on the star centerline.

- Star Wall Hip Location and Hip Angle

Four variables, XHIA, XLOF, XHIF, and XLOA were varied to move the hip up and down while holding the hip angle constant. The hip was moved up five inches and down eight inches without difficulty. Moving the hip up more than five inches causes cylinder one (CY1) to intersect cone one (CN1). This intersection is not taken into account in the computer code.

- Star Valley Floor Width

The width of the small plane forming the star valley floor was varied by changing the value of RBOTTP, which is the distance from the x-axis to the intersection of the star wall and the fillet in the star valley. To make the star valley plane equal to zero, RBOTTP was set to the fillet radius (FR), 1.62". No difficulty was encountered for RBOTTP between 1.875" and 1.62".

- Port Radius

The port radius was changed by varying the values of the first three elements of the array RI. The port radius can be varied over the range of ten to twenty inches. Values greater than twenty inches do not work since this brings the star peak very close to star hip location.

- Change Climbout Angle

The climbout angle of the transition region (α_4) was varied by changing the fourth element in the array AINCIN along with ZTO (the center of the torus). Aincin(4) and ZTO must be changed by equal amounts, i.e. if you add ten inches to AINCIN(4) then you must add ten inches to ZTO. When α_4 was changed, some small errors appeared which should not affect the numerical results of running the program. α_4 four was varied from ten to 50 degrees with no difficulty.

- Dimensions of the Transition Flare

The width of the transition is twice the value of WIDCO. WIDCO was increased and decreased by up to two inches without difficulty.

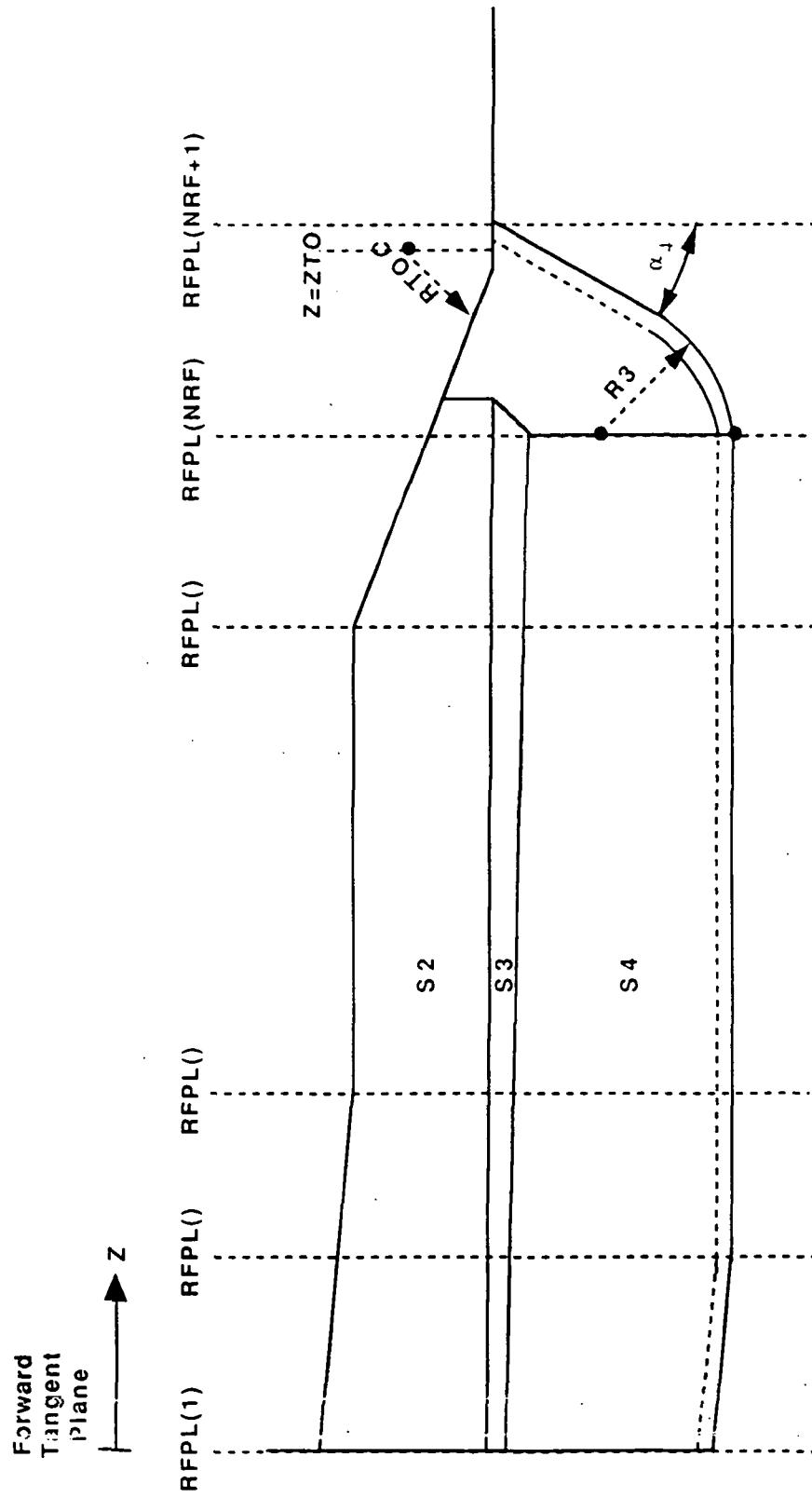
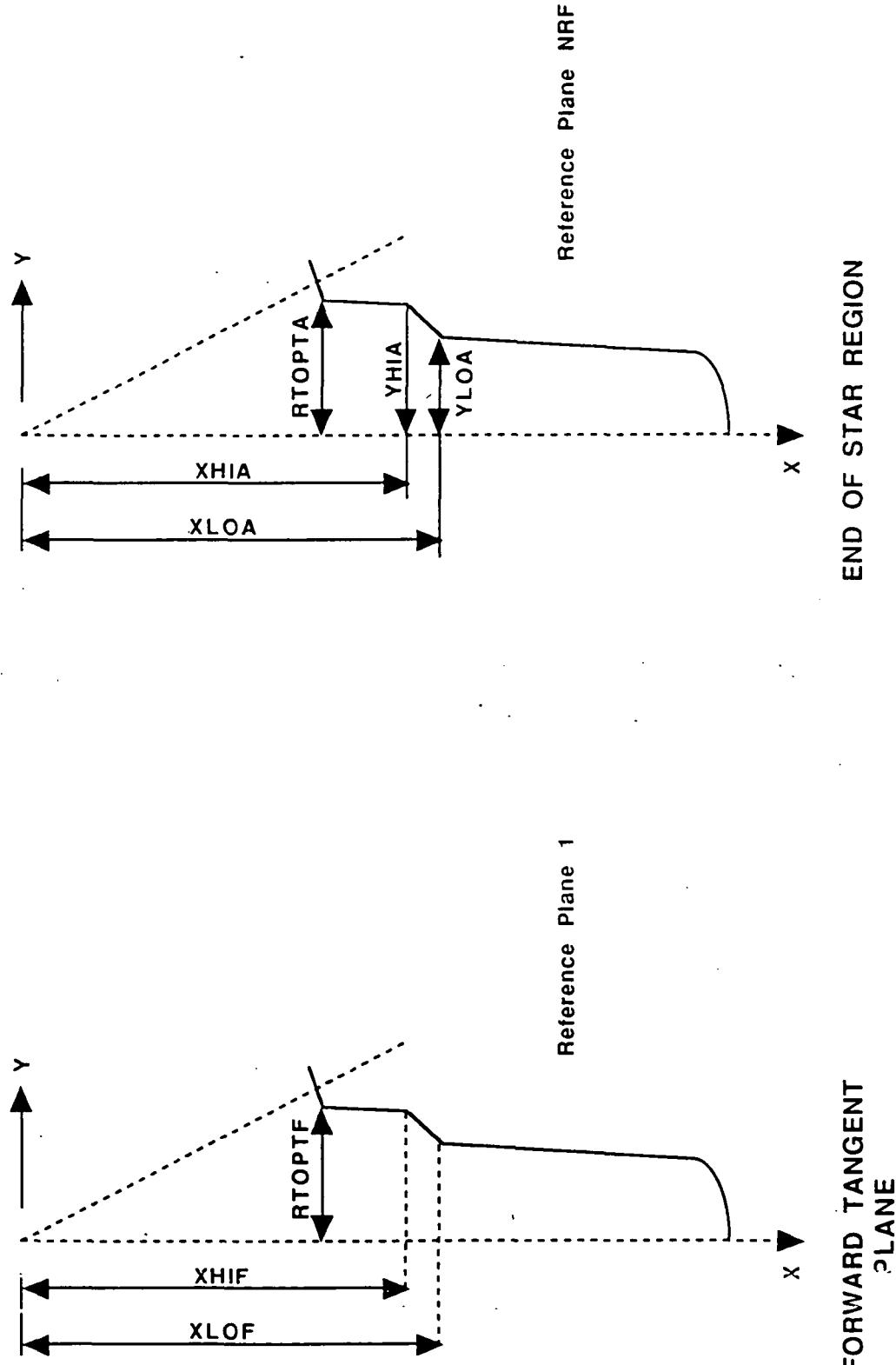


FIGURE A-1 LONGITUDINAL SECTION OF STAR AND TRANSITION REGIONS THROUGH THE VALLEY FLOOR

FIGURE A-2 STAR SECTION INPUT TO CBRM-A



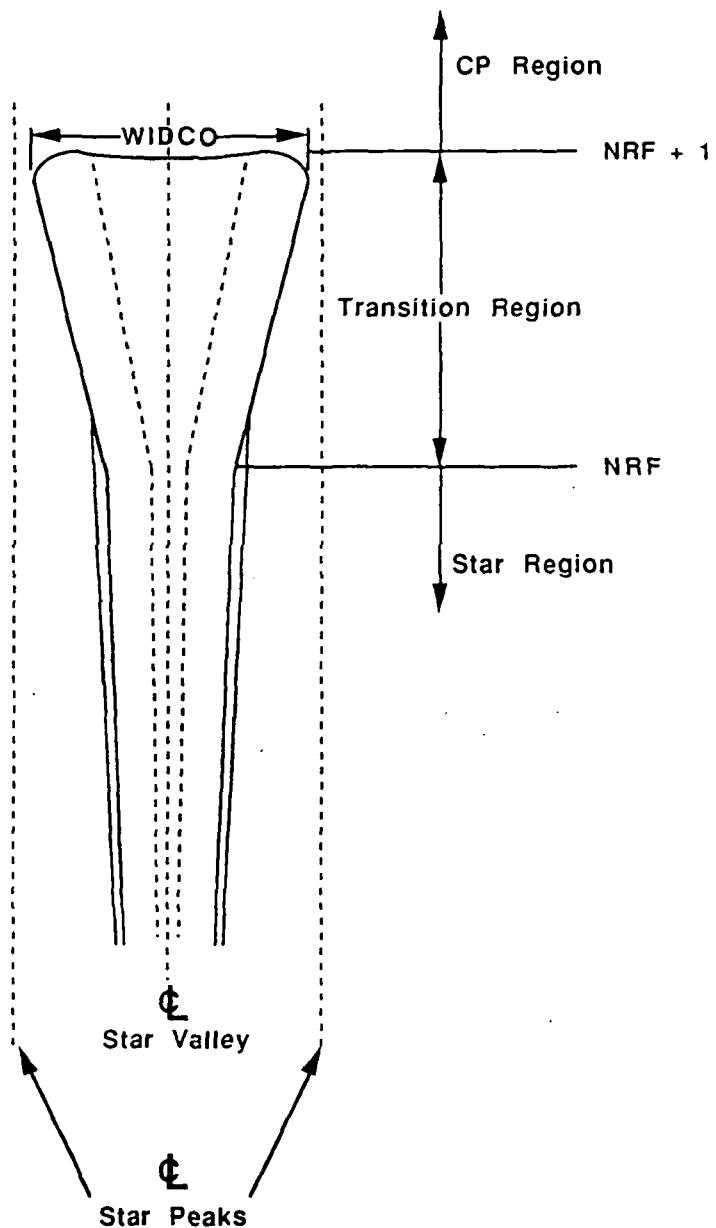


FIGURE A-3 VIEW FROM PORT OF TRANSITION REGION

LISTING OF PROGRAM INPUT - SAMPLE PROBLEM

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318.17, 323.314, 324.162, 350.0, 400.0, 434.89,
481.122, 483.345, 522.615, 637.322, 638.172,
643.312, 644.162, 650.0, 725.0, 788.722, 797.322,
798.172, 803.312, 804.162, 833.22, 915.771, 961.282,
963.522, 1057.792, 1150.0, 1253.207, 1283.507, 1289.627,
15*0.0,
RI= 3*17.0, 28.0, 28.787, 29.359, 29.366, 29.41, 29.417,
29.636, 30.061, 30.36, 30.75, 2*28.4, 29.1565, 29.1621,
29.1961, 29.2017, 29.24, 29.7366, 30.1582, 30.2151, 30.2208,
30.2548, 30.2604, 30.452, 30.9989, 31.3, 2*30.7, 35.5613,
41.0025, 42.6, 45.627, 15*0.0,
RVF=64.3, 2*66.2, 62.51, 28.787, 29.359, 29.366, 29.4095,
29.417, 29.636, 30.061, 30.36, 55.0, 28.4, 28.4,
29.1565, 29.1621,
29.1961, 29.2017, 29.24, 29.7366, 30.1582, 30.2151, 30.2208,
30.2548, 30.2604, 30.4527, 30.9989, 55.0, 30.7, 30.7, 35.5613,
41.0025, 42.6, 45.627, 15*0.0,
RF=71.854, 2*73.7, 74.3, 2*74.375, 74.317, 74.317, 3*74.375,
74.375, 68.000, 70.5, 2*74.375, 2*74.317,
4*74.375, 74.371, 74.313,
74.308, 74.366, 74.35, 74.317, 68.000, 70.12, 74.12, 73.728,
73.295, 72.674, 72.1910, 15*0.0,
DELTXF= 20.992, 20.333, 0.0, 0.0, 0.0,
DELTYF= 5.16, 5.161, 0.0, 0.0, 0.0,
TIF= .3, .3, 0.0, 0.0, 0.0,
DELTXA= 6.555, 7.019, 0.0, 0.0, 0.0,
DELTYA= 3.875, 4.0, 0.0, 0.0, 0.0,
TIA= 0.0, 0.0, 0.0, 0.0, 0.0,
ZAFT= 1289.627, 1292.383, 1299.507,
1313.507, 1331.762, 15*0.0,
AFTRI=45.627, 47.2181, 51.3, 51.65, 52.7,
15*0.0,
CIRAD= 20*0.0,
ZCORD= 1289.627, 1290.393, 1291.978, 1292.383, 1297.656,
1305.806, 1309.792, 1312.291, 1315.468, 1318.749, 1320.749,
1325.589, 1329.436, 1330.464, 1331.581, 1331.687, 1331.762,
33*0.0,
XCORD= 72.191, 72.103, 71.783, 71.668, 70.244, 68.402,
67.374, 66.529, 65.14, 63.356, 62.16, 58.779, 56.176, 55.009,
53.779, 53.149, 52.7, 33*0.0,
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NRF= 3,
KPLANE= 35,
RTOPTA= 3.0,
RTOPTF= 2.07337,
YHIA= 3.0,
YLOA= 1.875,

XHIA= 27.0,
XLOA= 29.0,
XHIF= 28.647,
XLOF= 29.0,
WIDCO= 6.0,
RBOTTP= 1.875,
R3= 4.0,
FR= 1.62,
DELZ= 20.0,
IISLOT= 13, 29, 3*0.0,
IDPNOZ= 2,
NOIDPS= 5,
NOCASE= 17,
NOCASA= 4,
TMAX= 100.0,
DTAU= 0.5,
NDUMP= 100,
NDUMPE= 0,
RANGLO= 0.0,
RANGHI= 0.0,
TSTART= 0.0,
RTO= 0.0,
ZTO= 157.31
\$END

5

LISTING OF PROGRAM OUTPUT - SAMPLE PROBLEM

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dtau = C.5C00000000000000
ndump = 100
ndumppe = 0
ranglo = 0.00000000000000E+00
ranghi = 0.00000000000000E+00
tstart = 0.00000000000000E+00
rto = C.0C000000000000E+00
zto = 157.310000000000
Send
END OF INPJT! DATA

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20.000000	17.000000	63.339264	72.447527	0.00000000E+00
40.000000	17.000000	63.998529	73.088055	0.00000000E+00
57.640000	17.000000	64.580000	73.653000	0.00000000E+00
77.640000	17.000000	64.580000	73.653000	0.00000000E+00
97.640000	17.000000	64.580000	73.653000	0.00000000E+00
117.640000	17.000000	64.580000	73.653000	0.00000000E+00
122.280000	17.000000	64.580000	73.653000	0.00000000E+00
142.280000	17.000000	64.580000	73.653000	0.00000000E+00
161.813000	28.000000	62.510000	74.253000	0.00000000E+00
181.813000	28.178478	28.178478	74.270009	0.00000000E+00
201.813000	28.356957	28.356957	74.287017	0.00000000E+00
221.813000	28.535435	28.535435	74.304026	0.00000000E+00
241.813000	28.713913	28.713913	74.321035	0.00000000E+00
256.003000	28.787000	28.787000	74.328000	0.00000000E+00
276.003000	28.956930	28.956930	74.328000	0.00000000E+00
296.003000	29.126859	29.126859	74.328000	0.00000000E+00
310.000000	29.296789	29.296789	74.328000	0.00000000E+00
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318.170000	29.366000	29.366000	74.270000	0.00000000E+00
323.314000	29.410000	29.410000	74.270000	0.00000000E+00
324.162000	29.417000	29.417000	74.328000	0.00000000E+00
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350.00000	29.636000	29.636000	74.328000	0.00000000E+00
370.00000	29.806000	29.806000	74.328000	0.00000000E+00
390.00000	29.976000	29.976000	74.328000	0.00000000E+00
400.00000	30.061000	30.061000	74.328000	0.00000000E+00
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434.89000	30.360000	30.360000	74.328000	0.00000000E+00
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602.61500	28.927605	28.927605	74.328000	0.00000000E+00
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7455.00000	29.868925	29.868925	74.328000	0.00000000E+00
7655.00000	30.001250	30.001250	74.328000	0.00000000E+00
7855.00000	30.133574	30.133574	74.328000	0.00000000E+00
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7955.32200	30.215100	30.215100	74.324000	0.00000000E+00
7992.17200	30.220800	30.220800	74.266000	0.00000000E+00
8033.31200	30.254800	30.254800	74.261000	0.00000000E+00
8044.16200	30.260400	30.260400	74.319000	0.00000000E+00
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8733.22200	30.717000	30.717000	74.287010	0.00000000E+00
8933.22200	30.849500	30.849500	74.279015	0.00000000E+00
9155.77100	30.998900	30.998900	74.270000	0.00000000E+00
9222.82639	31.045578	31.045578	73.942159	0.00000000E+00***
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9633.52200	30.700000	30.700000	70.073000	0.00000000E+00
9700.54100	30.700000	30.700000	74.073000	0.00000000E+00
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CPBURN VALUES----- PSIBAR= 6.2831852 PORT PERIMETER= 180.41483 PORT AREA= 2590.2079
CPBURN VALUES----- PSIBAR= 6.2831852 PORT PERIMETER= 180.87405 PORT AREA= 2603.4107
CPBURN VALUES----- PSIBAR= 6.2831852 PORT PERIMETER= 181.94175 PORT AREA= 2634.2372
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CPBURN VALUES----- PSIBAR= 6.2831852 PORT PERIMETER= 184.46803 PORT AREA= 2707.8985

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CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	184.83246	PORT AREA=	2718.6082
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	185.89757	PORT AREA=	2750.0309
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	186.20848	PORT AREA=	2759.2372
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CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	189.95574	PORT AREA=	2871.4086
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	190.75750	PORT AREA=	2895.6989
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	191.13133	PORT AREA=	2907.0593
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	178.44246	PORT AREA=	2533.8829
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	178.44246	PORT AREA=	2533.8829
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	179.27122	PORT AREA=	2557.4744
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	180.09998	PORT AREA=	2581.1751
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	180.92874	PORT AREA=	2604.9852
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	181.75750	PORT AREA=	2628.9046
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	182.58626	PORT AREA=	2652.9333
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	183.19569	PORT AREA=	2670.6726
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	183.23088	PORT AREA=	2671.6986
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	183.44450	PORT AREA=	2677.9320
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	183.47969	PORT AREA=	2678.9594

CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	183.72034	PORT AREA=	2685.9913
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	184.55240	PORT AREA=	2710.3759
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	185.38446	PORT AREA=	2734.8706
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	186.21652	PORT AREA=	2759.4756
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	186.84057	PORT AREA=	2778.0016
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	187.67199	PORT AREA=	2802.7802
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	188.50341	PORT AREA=	2827.6689
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	189.33483	PORT AREA=	2852.6676
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	189.48956	PORT AREA=	2857.3320
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	189.84707	PORT AREA=	2868.1241
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	189.88288	PORT AREA=	2869.2063
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	190.09651	PORT AREA=	2875.6660
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	190.13170	PORT AREA=	2876.7306
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	190.96029	PORT AREA=	2901.8587
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	191.33556	PORT AREA=	2913.2752
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	192.16808	PORT AREA=	2938.6823
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	193.00060	PORT AREA=	2964.1997
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	193.83312	PORT AREA=	2989.8274
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	194.77183	PORT AREA=	3018.8562
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	195.06512	PORT AREA=	3027.9547
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	192.89379	PORT AREA=	2960.9196
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	192.89379	PORT AREA=	2960.9196
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	192.89379	PORT AREA=	2960.9196

CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	192.89379	PORT AREA=	2960.9196
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	192.89379	PORT AREA=	2960.9196
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	192.89379	PORT AREA=	2960.9196
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	199.51890	PORT AREA=	3167.8036
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	206.14402	PORT AREA=	3381.6732
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	212.76914	PORT AREA=	3602.5285
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	219.39426	PORT AREA=	3830.3695
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	223.43823	PORT AREA=	3972.8770
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	230.06338	PORT AREA=	4211.9687
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	236.68852	PORT AREA=	4458.0460
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	243.31367	PORT AREA=	4711.1091
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	249.93881	PORT AREA=	4971.1578
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	256.56396	PORT AREA=	5238.1923
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	257.62630	PORT AREA=	5281.6612
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	264.25164	PORT AREA=	5556.8097
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	267.66369	PORT AREA=	5701.2366
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	286.68289	PORT AREA=	6540.2401
0.72144007D+04	0.71621000D+02	0.28395062D+00	0.43859395D+03	0.12923830D+04	0.47218100D+02	0.00000000D+00 0.00000000D+00
2	2	4	2	5	2	17 0.0000000D+00
0.12923837D+04	0.12896270D+04					
0.71621000D+02	0.69778651D+02	0.22601227D+00	0.36348318D+03	0.12995070D+04	0.51300000D+02	0.00000000D+00 0.00000000D+00
3	4	6	2	5	2	17 0.0000000D+00
0.1299507D+04	0.12923830D+04					
0.69778657D+02	0.65950359D+02	0.43720491D+00	0.64022207D+03	0.13135070D+04	0.51650000D+02	0.00000000D+00 0.00000000D+00
4	6	9	2	5	2	17 0.0000000D+00
0.1313507D+04	0.12995070D+04					

0.6595039102 0.527000000D+02 0.57518488D-01-0.23900937D+02 0.13331762D+04 0.527000000D+02 0.00000000D+00 0.00000000D+00
5 5 9 17 2 5 17 0.00000000D+00

0	0.13317620D+04	0.13135070D+04	0.0000000E+00	0.0000000E+00	0.0000000E+00
1	1289.6270	45.627000	1.0000000	0.0000000E+00	0.0000000E+00
2	1292.3830	47.218100	1.0000000	0.0000000E+00	0.57732221
3	1299.5070	51.300000	1.0000000	0.0000000E+00	0.57297866
4	1313.5070	51.650000	1.0000000	0.0000000E+00	0.2500000E-01
5	1331.7620	52.700000	1.0000000	0.0000000E+00	0.57518488E-01

URNOUT POINT CALCULATED AT 1331.7620 WITH PORT RADIUS AT 52.700000 .
THE VALUE WAS USED ONLY IF THE POSITION DID NOT COINCIDE WITH AN IDP .
DENIN VOLAFT AREAFT

2	928.22264	18660.771
3	2541.1988	54336.828
4	4529.3922	116539.27
5	5994.3400	156124.58
6	12054.031	1227000.67
7	18660.771	18660.771

***** BURNOUT BETWEEN PLANES 3 AND 2 *****
ARTIFICIAL PLANE SET AT 19.619784

CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	17237.320
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	17237.320
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	17237.320
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	17197.770
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	17158.267
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	17118.808
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	17079.395
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	17055.360
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	17016.536
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	16977.757
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	16939.022
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	16900.331
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	16861.684
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	16855.491
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	16667.370
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	16510.899
CPBURN VALUES-----	PSIBAR=	6.2831852	PORT PERIMETER=	0.0000000E+00 PORT AREA=	16351.225

PARAMETER SUMMARY-GRANIN DESIGN (THIOKOL) TC227/CDR

	FUEL SURFACE AREA--BETWEEN BOTH TANGENT PLANES--SQUARE INCHES	INCHES
1. 00000000E+00	411133.77	17.000000 376553.68
2. 50000000	414422.63	17.500000 373814.56
3. 00000000	418088.47	18.000000 371738.13
4. 50000000	421798.01	18.500000 370148.37
5. 00000000	425517.07	19.000000 368720.13
6. 50000000	429210.17	19.500000 367737.40
7. 00000000	432370.67	20.000000 368781.98
8. 50000000	434358.53	20.500000 371451.60
9. 00000000	435282.35	21.000000 373712.06
10. 50000000	435770.70	21.500000 376060.73
11. 50000000	436261.64	22.000000 378410.55
12. 50000000	437059.14	22.500000 380814.82
13. 00000000	438587.32	23.000000 383236.10
14. 50000000	440890.34	23.500000 385665.32
15. 00000000	444001.26	24.000000 388094.33
16. 50000000	441777.18	24.500000 390503.76
17. 00000000	4333849.77	25.000000 393038.96
18. 50000000	429555.67	25.500000 395496.62
19. 00000000	425976.29	26.000000 397983.36
20. 50000000	422850.78	26.500000 400475.25
21. 00000000	419960.13	27.000000 402896.82
22. 50000000	417169.47	27.500000 405376.25
23. 00000000	414380.89	28.000000 407772.50
24. 50000000	411711.01	28.500000 410138.58
25. 00000000	409186.05	29.000000 412486.46
26. 50000000	406615.92	29.500000 414831.70
27. 00000000	403993.04	30.000000 416840.46
28. 50000000	389993.29	30.500000 418761.39
29. 00000000	386645.02	31.000000 420701.48
30. 50000000	383181.49	31.500000 418245.34
31. 00000000	379902.60	32.000000 415456.38
		32.500000 412435.15
		33.000000 409249.47
		33.500000 406063.52

AFT END BURN AREA---A REGION---SQUARE INCHES			
.00000000E+00	928.22264	17.000000	2628.6998
.50000000	957.90854	17.500000	2696.8655
1.000000	989.10292	18.000000	2765.9518
1.500000	1021.7734	18.500000	2835.9539
2.000000	1055.8874	19.000000	2906.8675
2.500000	1091.4123	19.500000	2978.6885
3.000000	1128.3161	20.000000	3051.4128.
3.500000	1166.5675	20.500000	3125.0369
4.000000	1206.1366	21.000000	3199.5572
4.500000	1246.9944	21.500000	4333.2754
5.000000	1289.1132	22.000000	4077.5306
5.500000	1332.4670	22.500000	3827.1547
6.000000	1377.0309	23.000000	3581.5866
6.500000	1422.7815	23.500000	3333.7506
7.000000	1469.6969	24.000000	3083.6468
7.500000	1517.7563	24.500000	2831.2753
8.000000	1566.9406	25.000000	2576.6359
8.500000	1617.2314	25.500000	2319.7286
9.000000	1668.6120	26.000000	2066.5536
9.500000	1721.0664	26.500000	1799.1107
10.000000	1774.5800	27.000000	1535.4000
10.500000	1829.1390	27.500000	1271.8657
11.000000	1884.7304	28.000000	986.01372
11.500000	1941.3424	28.500000	691.31678
12.000000	1998.9637	29.000000	393.63757
12.500000	2057.5838	29.500000	56.383926
13.000000	2117.1931	30.000000	.00000000E+00
13.500000	2177.7824	30.500000	.00000000E+00
14.000000	2239.3432	31.000000	.00000000E+00
14.500000	2301.8676	31.500000	.00000000E+00
15.000000	2365.3482	32.000000	.00000000E+00
15.500000	2429.7780	32.500000	.00000000E+00
16.000000	2495.1505	33.000000	.00000000E+00
16.500000	2561.4597	33.500000	.00000000E+00

TOTAL BURN AREA---CYLINDRICAL+APT SECTIONS---SQUARE INCHES		
0.0000000E+00	425126.93	17.000000 384904.49
.5000000E+00	428539.46	17.500000 381404.48
1.000000E+00	432332.16	18.000000 378555.97
1.500000E+00	436060.06	18.500000 376182.93
2.000000E+00	439786.47	19.000000 373976.67
2.500000E+00	443486.89	19.500000 372320.54
3.000000E+00	446656.13	20.000000 372682.21
3.500000E+00	448651.28	20.500000 375050.76
4.000000E+00	449498.21	21.000000 377034.41
4.500000E+00	449896.07	21.500000 380394.01
5.000000E+00	450293.44	22.000000 382488.08
5.500000E+00	450994.28	22.500000 384641.97
6.000000E+00	452422.66	23.000000 386817.69
6.500000E+00	454624.53	23.500000 388999.07
7.000000E+00	457636.72	24.000000 391177.98
7.500000E+00	455310.82	24.500000 393335.04
8.000000E+00	447278.49	25.000000 395615.59
3.500000E+00	442876.36	25.500000 397816.35
9.000000E+00	439185.80	26.000000 400043.91
9.500000E+00	435945.97	26.500000 402274.36
10.000000E+00	432937.83	27.000000 404432.22
10.500000E+00	429988.89	27.500000 406648.11
11.000000E+00	427035.88	28.000000 408758.52
11.500000E+00	424188.90	28.500000 410829.90
12.000000E+00	421464.11	29.000000 412880.09
12.500000E+00	418689.95	29.500000 414888.09
13.000000E+00	415858.81	30.000000 416840.46
13.500000E+00	412336.77	30.500000 418761.39
14.000000E+00	408320.51	31.000000 420701.48
14.500000E+00	404468.89	31.500000 418245.34
15.000000E+00	400669.57	32.000000 415456.38
15.500000E+00	396860.38	32.500000 412435.15
16.000000E+00	392850.36	33.000000 409249.47
16.500000E+00	388927.80	33.500000 406063.52

FUEL SURFACE AREA---STAR REGION---SQUARE INCHES

.0C000000E+00	164871.55	17.000000	21210.265	34.000000
.5C000000	164642.13	17.500000	16192.811	34.500000
1.000000	164453.04	18.000000	11914.551	35.000000
1.500000	164287.77	18.500000	8057.6400	35.500000
2.000000	164144.30	19.000000	4473.3705	36.000000
2.500000	164020.25	19.500000	1200.1276	36.500000
3.000000	163317.66	20.000000	.00000000E+00	.00000000E+00
3.500000	161492.55	20.500000	.00000000E+00	.00000000E+00
4.000000	158650.22	21.000000	.00000000E+00	.00000000E+00
4.500000	155613.65	21.500000	.00000000E+00	.00000000E+00
5.000000	152586.72	22.000000	.00000000E+00	.00000000E+00
5.500000	149833.87	22.500000	.00000000E+00	.00000000E+00
6.000000	147824.43	23.000000	.00000000E+00	.00000000E+00
6.500000	146715.10	23.500000	.00000000E+00	.00000000E+00
7.000000	146317.91	24.000000	.00000000E+00	.00000000E+00
7.500000	140639.46	24.500000	.00000000E+00	.00000000E+00
8.000000	129570.97	25.000000	.00000000E+00	.00000000E+00
8.500000	121988.23	25.500000	.00000000E+00	.00000000E+00
9.000000	115153.34	26.000000	.00000000E+00	.00000000E+00
9.500000	108680.55	26.500000	.00000000E+00	.00000000E+00
10.000000	102422.76	27.000000	.00000000E+00	.00000000E+00
10.500000	96306.930	27.500000	.00000000E+00	.00000000E+00
11.000000	90291.269	28.000000	.00000000E+00	.00000000E+00
11.500000	84349.667	28.500000	.00000000E+00	.00000000E+00
12.000000	78464.751	29.000000	.00000000E+00	.00000000E+00
12.500000	72624.423	29.500000	.00000000E+00	.00000000E+00
13.000000	66819.952	30.000000	.00000000E+00	.00000000E+00
13.500000	61044.859	30.500000	.00000000E+00	.00000000E+00
14.000000	55294.220	31.000000	.00000000E+00	.00000000E+00
14.500000	49564.225	31.500000	.00000000E+00	.00000000E+00
15.000000	43851.872	32.000000	.00000000E+00	.00000000E+00
15.500000	38154.769	32.500000	.00000000E+00	.00000000E+00
16.000000	32470.981	33.000000	.00000000E+00	.00000000E+00
16.500000	26798.930	33.500000	.00000000E+00	.00000000E+00

	FUEL SURFACE AREA---TRANSITION REGION---SQUARE INCHES	
.0C000000E+00	12937.703	17.000000 9262.0580
.5C000000	13163.476	17.500000 8850.3271
1.C000000	13406.391	18.000000 8358.5537
1.5000000	13674.231	18.500000 7931.3417
2.C000000	13934.841	19.000000 7394.3447
2.5000000	14155.110	19.500000 6994.7858
3.0000000	14426.372	20.000000 6553.6419
3.5000000	14652.548	20.500000 6542.6616
4.0000000	14836.949	21.000000 6128.6032
4.5000000	14785.153	21.500000 5809.5061
5.0000000	14731.352	22.000000 5498.8673
5.5000000	14715.072	22.500000 5250.4690
6.0000000	14691.091	23.000000 5027.2656
6.5000000	14546.887	23.500000 4820.5225
7.0000000	14503.465	24.000000 4646.8874
7.5000000	14411.337	24.500000 4475.7920
8.0000000	14010.963	25.000000 4347.4844
8.5000000	13763.178	25.500000 4184.0141
9.0000000	13487.291	26.000000 4057.4249
9.5000000	13308.214	26.500000 3941.1716
10.000000	13154.014	27.000000 3759.4225
10.500000	12962.892	27.500000 3640.3973
11.000000	12678.705	28.000000 3505.2441
11.500000	12444.200	28.500000 3406.6767
12.000000	12302.952	29.000000 3296.4223
12.500000	12076.985	29.500000 3187.1056
13.000000	11767.442	30.000000 3075.6346
13.500000	11522.834	30.500000 2949.2036
14.000000	11266.016	31.000000 2849.3856
14.500000	10969.547	31.500000 2745.9361
15.000000	10679.872	32.000000 2653.0804
15.500000	10411.540	32.500000 2511.2582
16.000000	9982.0631	33.000000 2423.9924
16.500000	9705.0740	33.500000 2350.0660

	FUEL SURFACE AREA--SLOT	REGION NUMBER ONE--SQUARE INCHES
.0C000000E+00	14062.054	16266.213
.50000000	14099.219	16034.568
1.00000000	14297.136	15805.725
1.50000000	14493.521	15578.287
2.00000000	14688.375	15351.199
2.50000000	14881.698	15123.644
3.00000000	15073.489	14894.984
3.50000000	15263.749	20.000000
4.00000000	15452.478	20.500000
4.50000000	15639.675	21.000000
5.00000000	15825.341	21.500000
5.50000000	16009.476	22.000000
6.00000000	16192.079	22.500000
6.50000000	16373.151	23.000000
7.00000000	16552.692	23.500000
7.50000000	16730.701	24.000000
8.00000000	16907.179	24.500000
8.50000000	17082.126	25.000000
9.00000000	17255.542	26.000000
9.50000000	17427.426	26.500000
10.00000000	17597.779	27.000000
10.50000000	17766.600	27.500000
11.00000000	17933.890	28.000000
11.50000000	18099.649	28.500000
12.00000000	18263.877	29.000000
12.50000000	18426.573	29.500000
13.00000000	18587.738	30.000000
13.50000000	18368.902	30.500000
14.00000000	17922.896	31.000000
14.50000000	17574.326	31.500000
15.00000000	17273.871	32.000000
15.50000000	17001.342	32.500000
16.00000000	16746.289	33.000000
16.50000000	16502.560	33.500000

	FUEL SURFACE AREA--1ST SEGMENT	CP REGION--SQUARE INCHES
.0C000000E+00	51431.153	17.000000 78207.430
.52252.421	17.500000 78959.195	34.000000
1.0000000	18.000000 79708.916	34.500000
1.5000000	18.500000 80456.593	35.000000
2.0000000	19.000000 81202.225	35.500000
2.5000000	19.500000 81945.814	36.000000
3.0000000	20.000000 82687.358	36.500000
3.5000000	20.500000 83426.859	37.000000
4.0000000	21.000000 84164.315	37.500000
4.5000000	21.500000 84899.728	38.000000
5.0000000	22.000000 85633.096	38.500000
5.5000000	22.500000 86364.421	39.000000
6.0000000	23.000000 87093.701	39.500000
6.5000000	23.500000 87820.938	40.000000
7.0000000	24.000000 88546.130	40.500000
7.5000000	24.500000 89269.278	41.000000
8.0000000	25.000000 89990.383	41.500000
8.5000000	25.500000 90709.444	42.000000
9.0000000	26.000000 91426.460	42.500000
9.5000000	26.500000 92141.433	43.000000
10.000000	27.000000 92854.361	43.500000
10.500000	27.500000 93565.246	44.000000
11.000000	28.000000 94274.087	44.500000
11.500000	28.500000 94980.884	45.000000
12.000000	29.000000 95685.637	46.000000
12.500000	29.500000 96388.346	46.500000
13.000000	30.000000 97089.011	47.000000
13.500000	30.500000 97787.633	47.500000
14.000000	31.000000 98484.210	48.000000
14.500000	31.500000 99178.744	48.500000
15.000000	32.000000 99871.234	49.000000
15.500000	32.500000 100561.68	49.500000
16.000000	33.000000 101250.08	50.000000
16.500000	33.500000 101936.44	50.000000

	COLUMN #5 ON THE PLOT FILE	V06+V07+V08+V09
.00000000E+00	243302.46	17.000000 124945.97
.5C000000	244157.25	17.500000 120036.90
.1.0200000	245228.21	18.000000 115787.75
1.5000000	246344.35	18.500000 112023.86
2.0300000	247471.48	19.000000 108421.14
2.5000000	248574.11	19.500000 105264.37
3.0000000	249145.62	20.000000 104135.98
3.5000000	249854.94	20.500000 104634.23
4.0000000	246883.70	21.000000 104725.31
4.5000000	244787.45	21.500000 104906.94
5.0000000	242695.25	22.000000 105092.33
5.5000000	240911.08	22.500000 105335.03
6.0000000	239859.05	23.000000 105597.78
6.5000000	239583.31	23.500000 105871.69
7.0000000	240116.94	24.000000 106173.27
7.5000000	235317.02	24.500000 106414.12
8.0000000	224815.23	25.000000 106795.51
8.5000000	217948.21	25.500000 107101.58
9.0000000	211797.37	26.000000 107437.99
9.5200000	206101.85	26.500000 107780.72
10.000000	200642.65	27.000000 108054.38
10.500000	195284.90	27.500000 108387.24
11.000000	189930.68	28.000000 108700.39
11.500000	184696.62	28.500000 108987.90
12.000000	179608.94	29.000000 109257.71
12.500000	174477.54	29.500000 109525.64
13.000000	169294.86	30.000000 109788.39
13.500000	163824.44	30.500000 110032.97
14.000000	158137.05	31.000000 110300.81
14.500000	152526.04	31.500000 110561.51
15.000000	146985.55	32.000000 110829.16
15.500000	141507.52	32.500000 111044.09
16.000000	135897.10	33.000000 111309.71
16.500000	130460.19	33.500000 111584.71

	FUEL SURFACE AREA--2ND SEGMENT	CP REGION--SQUARE INCHES
.0C000000E+00	81747.473	17.000000 128690.29
.5C000000	83128.144	17.500000 130070.96
1.000000	84508.815	18.000000 131451.63
1.500000	85889.486	18.500000 132832.30
2.000000	87270.157	19.000000 134212.97
2.500000	88650.828	19.500000 135593.64
3.000000	90031.499	20.000000 136974.31
3.500000	91412.170	20.500000 138354.99
4.000000	92792.841	21.000000 139735.66
4.500000	94173.512	21.500000 141116.33
5.000000	95554.183	22.000000 142497.00
5.500000	96934.854	22.500000 143877.67
6.000000	98315.525	23.000000 145258.34
6.500000	99696.196	23.500000 146639.01
7.000000	101076.87	24.000000 148019.68
7.500000	102457.54	24.500000 149400.35
8.000000	103838.21	25.000000 150781.03
8.500000	105218.88	25.500000 152161.70
9.000000	106599.55	26.000000 153542.37
9.500000	107980.22	26.500000 154923.04
10.000000	109360.89	27.000000 156303.71
10.500000	110741.56	27.500000 157684.38
11.000000	112122.24	28.000000 159065.05
11.500000	113502.91	28.500000 160445.72
12.000000	114883.58	29.000000 161826.39
12.500000	116264.25	29.500000 163207.06
13.000000	117644.92	30.000000 164587.74
13.500000	119025.59	30.500000 165968.41
14.000000	120406.26	31.000000 167349.08
14.500000	121786.93	31.500000 168729.75
15.000000	123167.60	32.000000 170110.42
15.500000	124548.28	32.500000 171491.09
16.000000	125928.95	33.000000 172871.76
16.500000	127309.62	33.500000 174252.43

	FUEL SURFACE AREA--SLOT	REGION NUMBER	TWO--SQUARE' INCHES
.00000000E+00	13957.780	17.000000	15996.114
.50000000	13989.051	17.500000	15760.607
1.0000000	14181.065	18.000000	15527.805
1.5000000	14371.538	18.500000	15296.331
2.0000000	14560.472	19.000000	15065.148
2.5000000	14747.867	19.500000	14833.451
3.0000000	14933.721	20.000000	14600.610
3.5000000	15118.036	20.500000	14366.117
4.0000000	15300.811	21.000000	14129.563
4.5000000	15482.046	21.500000	13890.612
5.0000000	15661.741	22.000000	13648.984
5.5000000	15839.896	22.500000	13404.446
6.0000000	16016.512	23.000000	13156.802
6.5000000	16191.588	23.500000	12905.884
7.0000000	16365.124	24.000000	12627.045
7.5000000	16537.120	24.500000	12389.302
8.0000000	16707.577	25.000000	12136.724
3.5000000	16876.494	25.500000	11881.889
9.0000000	17043.871	26.000000	11625.748
9.5000000	17209.708	26.500000	11368.396
10.000000	17374.005	27.000000	11109.761
10.500000	17536.763	27.500000	10849.732
11.000000	17697.980	28.000000	10526.202
11.500000	17857.659	28.500000	10198.104
12.000000	18015.796	29.000000	9869.4648
12.500000	18172.395	29.500000	9540.0530
13.000000	18327.454	30.000000	9209.6647
13.500000	18111.744	30.500000	8878.1172
14.000000	17669.057	31.000000	8545.2474
14.500000	17319.802	31.500000	8210.9086
15.000000	17017.204	32.000000	7874.9689
15.500000	16741.808	32.500000	7537.3093
16.000000	16483.472	33.000000	7197.8221
16.500000	16236.192	33.500000	6856.4096

	COLUMN # 6 ON THE PLOT FILE	V16+V17
.0000000E+00	95705.253	17.000000 144686.40
.5000000	97117.195	17.500000 145831.57
1.0000000	98689.879	18.000000 146979.44
1.5000000	100261.02	18.500000 148128.63
2.0000000	101830.63	19.000000 149278.12
2.5000000	103398.69	19.500000 150427.09
3.0000000	104965.22	20.000000 151574.92
3.5000000	106530.21	20.500000 152721.10
4.0000000	108093.65	21.000000 153865.22
4.5000000	109655.56	21.500000 155006.94
5.0000000	111215.92	22.000000 156145.98
5.5000000	112774.75	22.500000 157282.12
6.0000000	114332.04	23.000000 158415.14
6.5000000	115887.78	23.500000 159544.90
7.0000000	117441.99	24.000000 160646.73
7.5000000	118994.66	24.500000 161789.66
8.0000000	120545.79	25.000000 162917.75
8.5000000	122095.37	25.500000 164043.59
9.0000000	123643.42	26.000000 165168.12
9.5000000	125189.93	26.500000 166291.43
10.000000	126734.90	27.000000 167413.47
10.500000	128278.33	27.500000 168534.11
11.000000	129820.22	28.000000 169591.25
11.500000	131360.57	28.500000 170643.83
12.000000	132899.37	29.000000 171695.86
12.500000	134436.64	29.500000 172747.12
13.000000	135972.37	30.000000 173797.40
13.500000	137137.34	30.500000 174846.52
14.000000	138075.32	31.000000 175894.33
14.500000	139106.74	31.500000 176940.66
15.000000	140184.81	32.000000 177985.39
15.500000	141290.08	32.500000 179028.40
16.000000	142412.42	33.000000 180069.58
16.500000	143545.81	33.500000 181108.84

	FUEL SURFACE AREA--3RD SEGMENT	CP REGION--SQUARE	INCHES
.00000000E+00	72126.061	17.000000	106921.31
.50000000	73148.188	17.500000	107946.09
1.00000000	74170.380	18.000000	108970.95
1.50000000	75192.639	18.500000	109995.88
2.00000000	76214.967	19.000000	111020.87
2.50000000	77237.366	19.500000	112045.94
3.00000000	78259.837	20.000000	113071.07
3.50000000	79282.380	20.500000	114096.27
4.00000000	80304.999	21.000000	115121.53
4.50000000	81327.692	21.500000	116146.85
5.00000000	82350.463	22.000000	117172.23
5.50000000	83373.312	22.500000	118197.68
6.00000000	84396.239	23.000000	119223.17
6.50000000	85419.246	23.500000	120248.73
7.00000000	86442.334	24.000000	121274.33
7.50000000	87465.503	24.500000	122299.99
8.00000000	88488.753	25.000000	123325.70
8.50000000	89512.086	25.500000	124351.45
9.00000000	90535.502	26.000000	125377.25
9.50000000	91559.000	26.500000	126403.09
10.00000000	92582.582	27.000000	127428.97
10.50000000	93606.246	27.500000	128454.90
11.00000000	94629.994	28.000000	129480.86
11.50000000	95653.825	28.500000	130506.85
12.00000000	96677.739	29.000000	131532.88
12.50000000	97701.735	29.500000	132558.95
13.00000000	98725.813	30.000000	133254.68
13.50000000	99749.973	30.500000	133881.89
14.00000000	100774.21	31.000000	134506.34
14.50000000	101798.53	31.500000	130743.17
15.00000000	102822.94	32.000000	126641.84
15.50000000	103847.41	32.500000	122362.66
16.00000000	104871.97	33.000000	117870.18
16.50000000	105896.60	33.500000	113369.97

	COLUMN #7 ON THE PLOT FILE	V18+V19
0.0000000E+00	72126.061	17.000000 106921.31
.5000000E+00	73148.188	17.500000 107946.09
1.0000000E+00	74170.380	18.000000 108970.95
1.5000000E+00	75192.639	18.500000 109955.88
2.0000000E+00	76214.967	19.000000 111020.87
2.5000000E+00	77237.366	19.500000 112045.94
3.0000000E+00	78259.837	20.000000 113071.07
3.5000000E+00	79282.380	20.500000 114096.27
4.0000000E+00	80304.999	21.000000 115121.53
4.5000000E+00	81327.692	21.500000 116146.85
5.0000000E+00	82350.463	22.000000 117172.23
5.5000000E+00	83373.312	22.500000 118197.68
6.0000000E+00	84396.239	23.000000 119223.17
6.5000000E+00	85419.246	23.500000 120248.73
7.0000000E+00	86442.334	24.000000 121274.33
7.5000000E+00	87465.503	24.500000 122299.99
8.0000000E+00	88488.753	25.000000 123325.70
8.5000000E+00	89512.086	25.500000 124351.45
9.0000000E+00	90535.502	26.000000 125377.25
9.5000000E+00	91559.000	26.500000 126403.09
10.000000E+00	92582.582	27.000000 127428.97
10.500000E+00	93606.246	27.500000 128454.90
11.000000E+00	94629.994	28.000000 129480.86
11.500000E+00	95653.825	28.500000 130506.85
12.000000E+00	96677.739	29.000000 131532.88
12.500000E+00	97701.735	29.500000 132558.95
13.000000E+00	98725.813	30.000000 133254.68
13.500000E+00	99749.973	30.500000 133881.89
14.000000E+00	100774.21	31.000000 134506.34
14.500000E+00	101798.53	31.500000 13543.17
15.000000E+00	102822.94	32.000000 126541.84
15.500000E+00	103847.41	32.500000 122362.66
16.000000E+00	104871.97	33.000000 117870.18
16.500000E+00	105896.60	33.500000 113369.97

	AFT END BURN AREA--TOTAL--SQUARE INCHES	
1. 00000000E+00	13993.154	17.000000 8350.8078
.50000000	14116.825	17.500000 7589.9191
1. 00000000	14243.690	18.000000 6817.8384
1. 50000000	14262.052	18.500000 6034.5611
2. 00000000	14269.401	19.000000 5256.5363
2. 50000000	14276.725	19.500000 4583.1391
3. 00000000	14285.462	20.000000 3900.2303
3. 50000000	14292.754	20.500000 3599.1596
4. 00000000	14215.856	21.000000 3322.3480
4. 50000000	14125.310	21.500000 4333.2754
5. 00000000	14031.805	22.000000 4077.5306
5. 50000000	13935.134	22.500000 3827.1547
6. 00000000	13835.333	23.000000 3581.5866
6. 50000000	13734.186	23.500000 3333.7506
7. 00000000	13635.452	24.000000 3083.6468
7. 50000000	13533.637	24.500000 2831.2753
8. 00000000	13428.720	25.000000 2576.6359
8. 50000000	13320.685	25.500000 2319.7286
9. 00000000	13209.513	26.000000 2060.5536
9. 50000000	13095.190	26.500000 1799.1107
10. 00000000	12977.700	27.000000 1535.4000
10. 50000000	12819.423	27.500000 1271.8657
11. 00000000	12654.992	28.000000 986.01372
11. 50000000	12477.887	28.500000 691.31678
12. 00000000	12278.061	29.000000 393.63757
12. 50000000	12074.025	29.500000 56.383926
13. 00000000	11865.769	30.000000 .00000000E+00
13. 50000000	11625.025	30.500000 .00000000E+00
14. 00000000	11333.930	31.000000 .00000000E+00
14. 50000000	11037.579	31.500000 .00000000E+00
15. 00000000	10676.280	32.000000 .00000000E+00
15. 50000000	10215.364	32.500000 .00000000E+00
16. 00000000	9668.8666	33.000000 .00000000E+00
16. 50000000	9025.2010	33.500000 .00000000E+00

	COLUMN #8 ON THE PLOT FILE	V20,V21+V30
.0000000E+00	13993.154	17.000000 8350.8078 .0000000E+00
.5000000	14116.825	17.500000 7589.9191 .0000000E+00
1.0000000	14243.690	18.000000 6817.8384 .0000000E+00
1.5000000	14262.052	18.500000 6034.5611 .0000000E+00
2.0000000	14269.401	19.000000 5256.5363 .0000000E+00
2.5000000	14276.725	19.500000 4583.1391 .0000000E+00
3.0000000	14285.462	20.000000 3900.2303 .0000000E+00
3.5000000	14292.754	20.500000 3599.1596 .0000000E+00
4.0000000	14215.856	21.000000 3322.3480 .0000000E+00
4.5000000	14125.370	21.500000 4333.2754 .0000000E+00
5.0000000	14031.805	22.000000 4077.5306 .0000000E+00
5.5000000	13935.134	22.500000 3827.1547 .0000000E+00
6.0000000	13835.333	23.000000 3581.5866 .0000000E+00
6.5000000	13734.186	23.500000 3333.7506 .0000000E+00
7.0000000	13635.452	24.000000 3083.6468 .0000000E+00
7.5000000	13533.637	24.500000 2831.2753 .0000000E+00
8.0000000	13428.720	25.000000 2576.6359 .0000000E+00
8.5000000	13320.685	25.500000 2319.7286 .0000000E+00
9.0000000	13220.513	26.000000 2060.5536 .0000000E+00
9.5000000	13095.190	26.500000 1799.1107 .0000000E+00
10.000000	12977.700	27.000000 1535.4000 .0000000E+00
10.500000	12819.423	27.500000 1271.8657 .0000000E+00
11.000000	12654.992	28.000000 986.013772 .0000000E+00
11.500000	12477.887	28.500000 691.31678 .0000000E+00
12.000000	12278.061	29.000000 393.63757 .0000000E+00
12.500000	12074.025	29.500000 56.383926 .0000000E+00
13.000000	11865.769	30.000000 .0000000E+00 .0000000E+00
13.500000	11625.025	30.500000 .0000000E+00 .0000000E+00
14.000000	11333.930	31.000000 .0000000E+00 .0000000E+00
14.500000	11037.579	31.500000 .0000000E+00 .0000000E+00
15.000000	10676.280	32.000000 .0000000E+00 .0000000E+00
15.500000	10215.364	32.500000 .0000000E+00 .0000000E+00
16.000000	9668.8664	33.000000 .0000000E+00 .0000000E+00
16.500000	9025.2010	33.500000 .0000000E+00 .0000000E+00

*** END PROGRAM CBRM ***